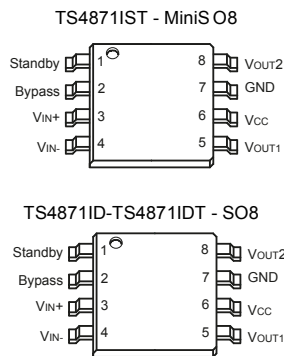


Output rail-to-rail 1 W audio power amplifier with standby mode



Features

- Operating from $V_{CC} = 2.5\text{ V}$ to 5.5 V
- 1 W rail-to-rail output power @ $V_{CC} = 5\text{ V}$, THD = 1%, $f = 1\text{ kHz}$, with $8\ \Omega$ load
- Ultra low consumption in standby mode (10 nA)
- 75 dB PSRR @ 217 Hz from 5 V to 2.6 V
- Ultra low pop and click
- Ultra low distortion (0.1%)
- Unity gain stable
- Available in SO8 and MiniSO8

Applications

- Mobile phones (cellular / cordless)
- Laptop / notebook computers
- PDAs
- Portable audio devices

Description

The **TS4871** is an audio power amplifier capable of delivering 1 W of continuous RMS output power into $8\ \Omega$ load @ 5 V.

This audio amplifier exhibits 0.1% distortion level (THD) from a 5 V supply for a $P_{out} = 250\text{ mW}$ RMS. An external standby mode control reduces the supply current to less than 10 nA. An internal thermal shutdown protection is also provided.

The **TS4871** has been designed for high quality audio applications such as mobile phones and to minimize the number of external components.

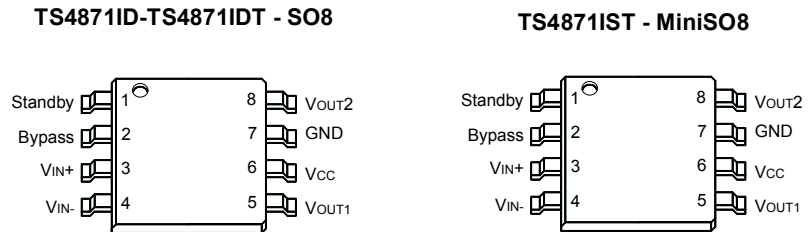
The unity-gain stable amplifier can be configured by external gain setting resistors.

Product status link

[TS4871](#)

1 Pin configuration

Figure 1. Pin connections (top view)



2 Maximum ratings

Table 1. Absolute maximum ratings

| Symbol | Parameter | Value | Unit |
|------------|--|-----------------------------------|------|
| V_{CC} | Supply voltage ⁽¹⁾ | 6 | V |
| V_i | Input voltage ⁽²⁾ | GND to V_{CC} | V |
| T_{oper} | Operating free air temperature range | -40 to + 85 | °C |
| T_{stg} | Storage temperature | -65 to +150 | °C |
| T_j | Maximum junction temperature | 150 | °C |
| R_{thja} | Thermal resistance junction-to-ambient ⁽³⁾ SO8 | 175 | °C/W |
| | Thermal resistance junction-to-ambient ⁽³⁾ MiniSO8 | 215 | |
| P_d | Power dissipation | Internally limited ⁽⁴⁾ | |
| ESD | Human body model | 2 | kV |
| ESD | Machine model | 200 | V |
| Latch-up | Latch-up immunity | Class A | |
| | Lead temperature (soldering, 10 s) | 260 | °C |

1. All voltages values are measured with respect to the ground pin.
2. The magnitude of input signal must never exceed $V_{CC} + 0.3 V / GND - 0.3 V$
3. The device is protected in case of overtemperature by a thermal shutdown active @ 150 °C.
4. Exceeding the power derating curves during a long period, involves abnormal operating conditions.

Table 2. Operating conditions

| Symbol | Parameter | Value | Unit |
|------------|--|---|----------|
| V_{CC} | Supply voltage | 2.5 to 5.5 | V |
| V_{ICM} | Common mode Input voltage range | GND to $V_{CC} - 1.2 V$ | V |
| V_{STB} | Standby voltage input: device ON | $GND \leq V_{STB} \leq 0.5 V$ | V |
| | Standby voltage input: device OFF | $V_{CC} - 0.5 V \leq V_{STB} \leq V_{CC}$ | |
| R_L | Load resistor | 4 - 32 | Ω |
| R_{thja} | Thermal resistance junction-to-ambient ⁽¹⁾ SO8 | 150 | °C/W |
| | Thermal resistance junction-to-ambient ⁽¹⁾ MiniSO8 | 190 | |

1. This thermal resistance can be reduced with a suitable PCB layout (see power derating curves).

3 Electrical characteristics

Table 3. Electrical characteristics $V_{CC} = +5\text{ V}$, $GND = 0\text{ V}$, $T_{amb} = 25\text{ °C}$ (unless otherwise specified).

| Symbol | Parameter | Min. | Typ. | Max. | Unit |
|---------------------|---|------|------|------|---------|
| I_{CC} | Supply current No input signal, no load | | 6 | 8 | mA |
| $I_{STANDBY}^{(1)}$ | Standby current No input signal, $V_{STDBY} = V_{CC}$, $R_L = 8\ \Omega$ | | 10 | 1000 | nA |
| V_{OO} | Output offset voltage No input signal, $R_L = 8\ \Omega$ | | 5 | 20 | mV |
| P_O | Output power THD = 1% max., $f = 1\text{ kHz}$, $R_L = 8\ \Omega$ | | 1 | | W |
| THD + N | Total harmonic distortion + noise $P_O = 250\text{ mW}_{rms}$, $G_v = 2$, $20\text{ Hz} < f < 20\text{ kHz}$, $R_L = 8\ \Omega$ | | 0.15 | | % |
| PSRR ⁽²⁾ | Power supply rejection ratio $f = 217\text{ Hz}$, $R_L = 8\ \Omega$, $R_{Feed} = 22\text{ K}$, $V_{ripple} = 200\text{ mV}_{rms}$ | | 75 | | dB |
| ϕ_M | Phase margin at unity gain $R_L = 8\ \Omega$, $C_L = 500\text{ pF}$ | | 70 | | Degrees |
| GM | Gain margin $R_L = 8\ \Omega$, $C_L = 500\text{ pF}$ | | 20 | | dB |
| GBP | Gain bandwidth product $R_L = 8\ \Omega$ | | 2 | | MHz |

1. Standby mode is activated when V_{stdby} is tied to V_{CC} .

2. Dynamic measurements - $20 \cdot \log(rms(V_{out})/rms(V_{ripple}))$. V_{ripple} is the surimposed sinus signal to V_{CC} @ $f = 217\text{ Hz}$.

Table 4. Electrical characteristics $V_{CC} = +3.3\text{ V}$, $GND = 0\text{ V}$, $T_{amb} = 25\text{ °C}$ (unless otherwise specified)

| Symbol | Parameter | Min. | Typ. | Max. | Unit |
|---------------------|---|------|------|------|---------|
| I_{CC} | Supply current No input signal, no load | | 5.5 | 8 | mA |
| $I_{STANDBY}^{(1)}$ | Standby current No input signal, $V_{STDBY} = V_{CC}$, $R_L = 8\ \Omega$ | | 10 | 1000 | nA |
| V_{OO} | Output offset voltage No input signal, $R_L = 8\ \Omega$ | | 5 | 20 | mV |
| P_O | Output power THD = 1% max., $f = 1\text{ kHz}$, $R_L = 8\ \Omega$ | | 450 | | mW |
| THD + N | Total harmonic distortion + noise $P_O = 250\text{ mW}_{rms}$, $G_v = 2$, $20\text{ Hz} < f < 20\text{ kHz}$, $R_L = 8\ \Omega$ | | 0.15 | | % |
| PSRR ⁽²⁾ | Power supply rejection ratio $f = 217\text{ Hz}$, $R_L = 8\ \Omega$, $R_{Feed} = 22\text{ k}\Omega$, $V_{ripple} = 200\text{ mV}_{rms}$ | | 75 | | dB |
| ϕ_M | Phase margin at unity gain $R_L = 8\ \Omega$, $C_L = 500\text{ pF}$ | | 70 | | Degrees |
| GM | Gain margin $R_L = 8\ \Omega$, $C_L = 500\text{ pF}$ | | 20 | | dB |
| GBP | Gain bandwidth product $R_L = 8\ \Omega$ | | 2 | | MHz |

1. Standby mode is activated when V_{stbby} is tied to V_{CC}

2. Dynamic measurements - $20 \cdot \log(\text{rms}(V_{out})/\text{rms}(V_{ripple}))$. V_{ripple} is the surimposed sinus signal to V_{CC} @ $f = 217\text{ Hz}$

Note: All electrical values are made by correlation between 2.6 V and 5 V measurements.

Table 5. Electrical characteristics $V_{CC} = +2.6\text{ V}$, $GND = 0\text{ V}$, $T_{amb} = 25\text{ °C}$ (unless otherwise specified).

| Symbol | Parameter | Min. | Typ. | Max. | Unit |
|---------------------|---|------|------|------|------|
| I_{CC} | Supply current No input signal, no load | | 5.5 | 8 | mA |
| $I_{STANDBY}^{(1)}$ | Standby current No input signal, $V_{STDBY} = V_{CC}$, $R_L = 8\ \Omega$ | | 10 | 1000 | nA |
| V_{OO} | Output offset voltage No input signal, $R_L = 8\ \Omega$ | | 5 | 20 | mV |
| P_O | Output power THD = 1% max., $f = 1\text{ kHz}$, $R_L = 8\ \Omega$ | | 260 | | mW |
| THD + N | Total harmonic distortion + noise $P_O = 250\text{ mW}_{rms}$, $G_v = 2$, $20\text{ Hz} < f < 20\text{ kHz}$, $R_L = 8\ \Omega$ | | 0.15 | | % |
| PSRR ⁽²⁾ | Power supply rejection ratio $f = 217\text{ Hz}$, $R_L = 8\ \Omega$, $R_{Feed} = 22\text{ k}\Omega$, $V_{ripple} = 200\text{ mV}_{rms}$ | | 75 | | dB |

| Symbol | Parameter | Min. | Typ. | Max. | Unit |
|----------|---|------|------|------|---------|
| ϕ_M | Phase margin at unity gain $R_L = 8 \Omega$, $C_L = 500 \text{ pF}$ | | 70 | | Degrees |
| GM | Gain margin $R_L = 8 \Omega$, $C_L = 500 \text{ pF}$ | | 20 | | dB |
| GBP | Gain bandwidth product $R_L = 8 \Omega$ | | 2 | | MHz |

- Standby mode is activated when V_{stdby} is tied to V_{CC}
- Dynamic measurements - $20 \cdot \log(\text{rms}(V_{out})/\text{rms}(V_{ripple}))$. V_{ripple} is the surimposed sinus signal to V_{CC} @ $f = 217 \text{ Hz}$

Table 6. Bill of material

| Components | Functional description |
|------------|--|
| R_{in} | Inverting input resistor which sets the closed loop gain in conjunction with R_{feed} . This resistor also forms a high pass filter with C_{in} [$f_c = 1 / (2 \times P_i \times R_{in} \times C_{in})$] |
| C_{in} | Input coupling capacitor which blocks the DC voltage at the amplifier input terminal |
| R_{feed} | Feed back resistor which sets the closed loop gain in conjunction with R_{in} |
| C_s | Supply bypass capacitor which provides power supply filtering |
| C_b | Bypass pin capacitor which provides half supply filtering |
| C_{feed} | Low pass filter capacitor allowing to cut the high frequency [low pass filter cut-off frequency $1 / (2 \times P_i \times R_{feed} \times C_{feed})$] |
| R_{stb} | Pull-up resistor which fixes the right supply level on the standby pin |
| G_v | Closed loop gain in BTL configuration = $2 \times (R_{feed} / R_{in})$ |

Remarks

- All measurements, except PSRR measurements, are made with a supply bypass capacitor $C_s = 100 \mu\text{F}$.
- External resistors are not needed for having better stability when supply @ V_{CC} down to 3 V. By the way, the quiescent current remains the same.
- The standby response time is about 1 μs .

4 Electrical characteristics curves

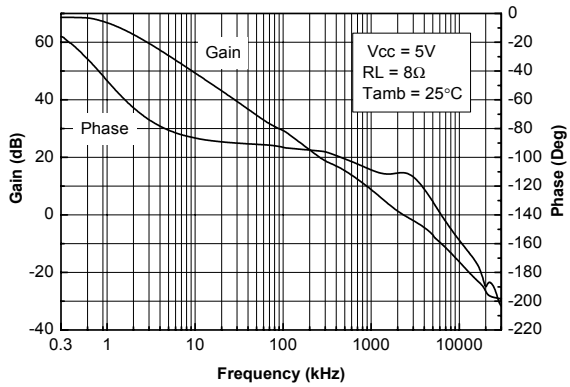
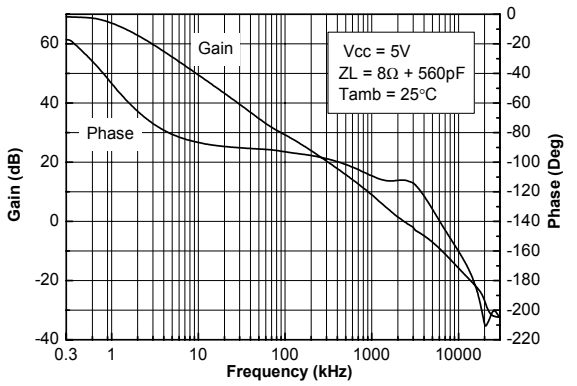
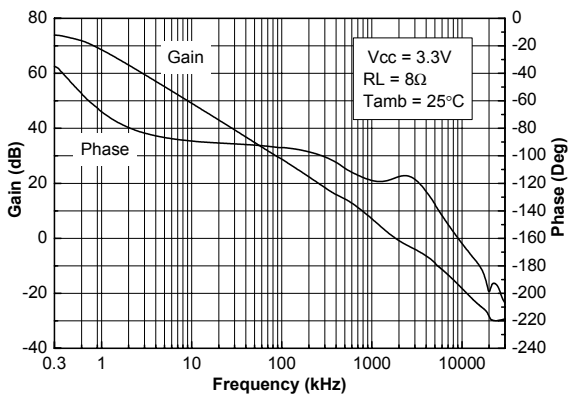
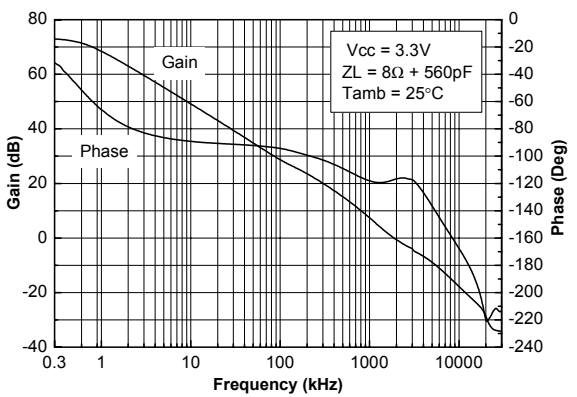
Figure 2. Open loop frequency response Vcc=5 V

Figure 3. Open loop frequency response ZL=8 Ω

Figure 4. Open loop frequency response Vcc=3.3 V

Figure 5. Open loop frequency response Vcc=3.3 V, ZL=8 Ω


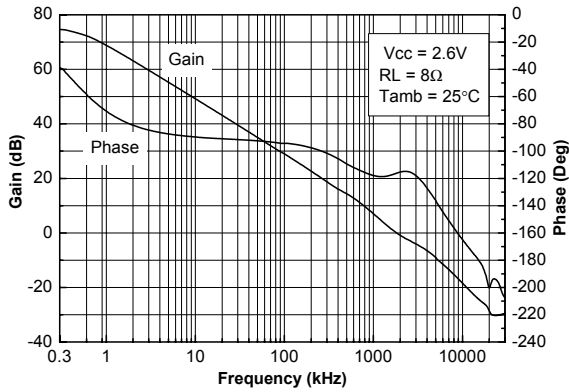
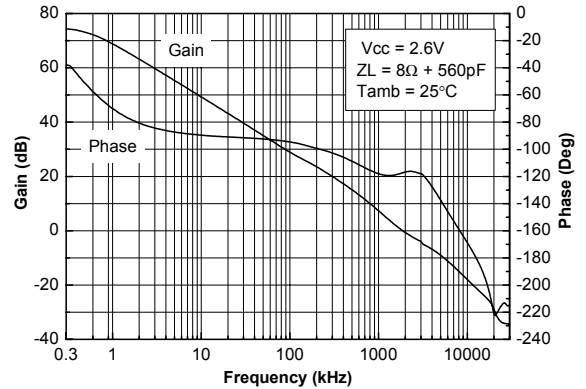
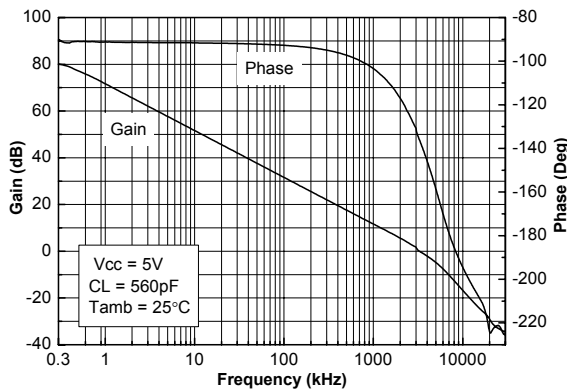
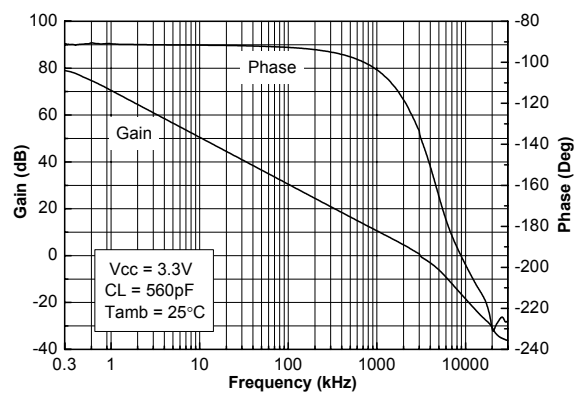
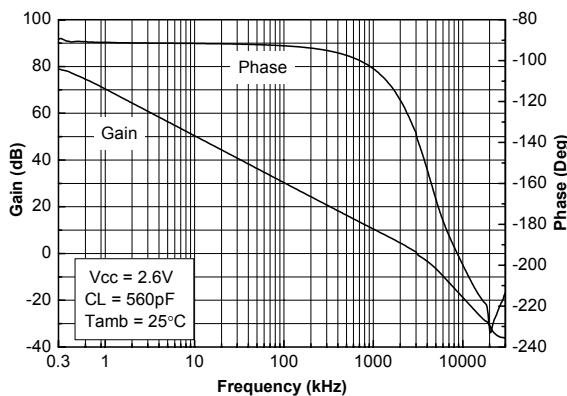
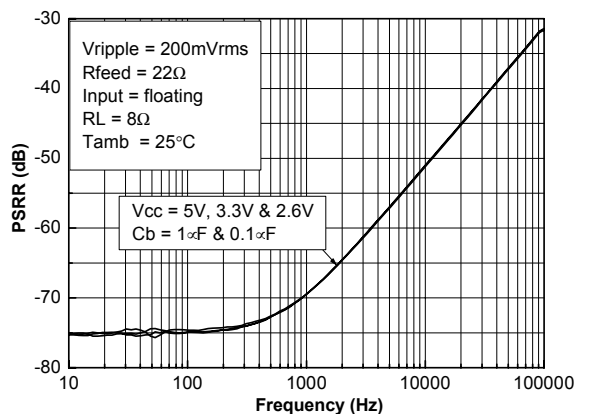
Figure 6. Open loop frequency response Vcc=2.6 V

Figure 7. Open loop frequency response Vcc=2.6 V, ZL=8 Ω

Figure 8. Open loop frequency response Vcc=5 V, CL=560 pF

Figure 9. Open loop frequency response Vcc=3.3 V, CL=560 pF

Figure 10. Open loop frequency response Vcc=2.6 V, CL=560 pF

Figure 11. Power supply rejection ratio (PSRR) vs power supply


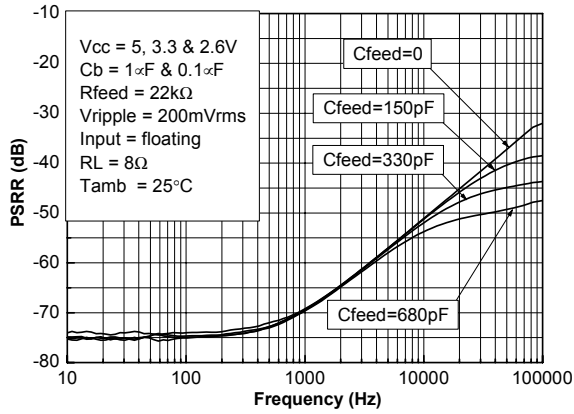
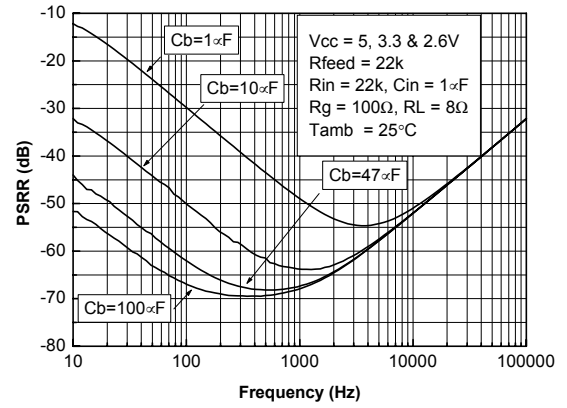
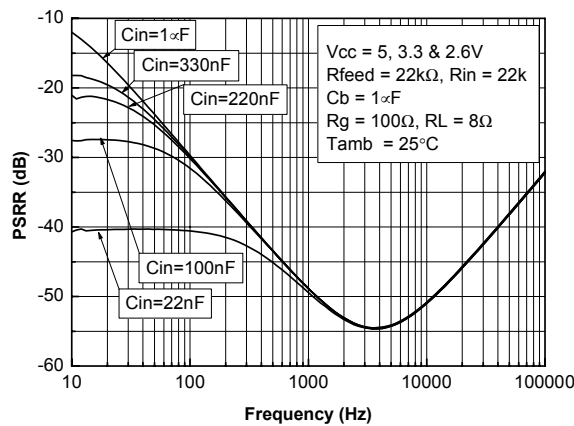
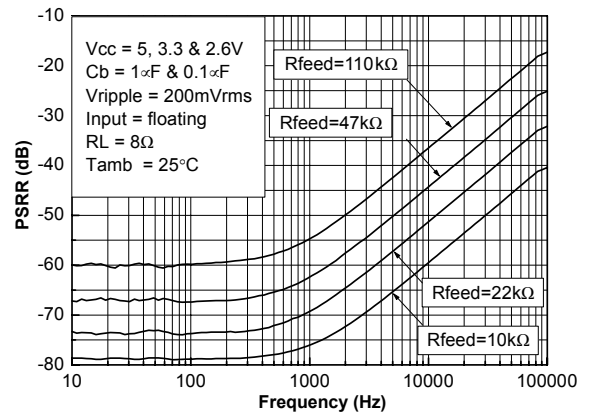
Figure 12. Power supply rejection ratio (PSRR) vs feedback capacitor

Figure 13. Power supply rejection ratio (PSRR) vs bypass capacitor

Figure 14. Power supply rejection ratio (PSRR) vs input capacitor

Figure 15. Power supply rejection ratio (PSRR) vs feedback resistor


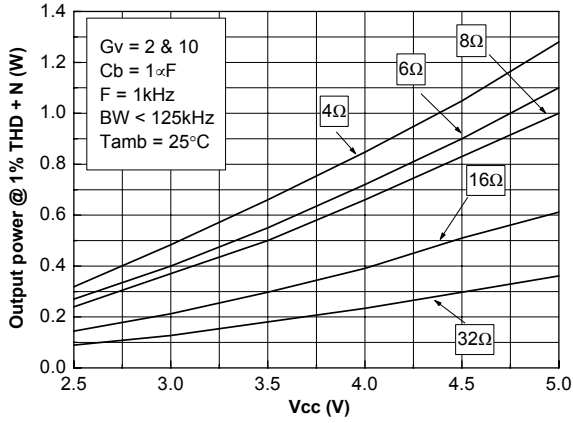
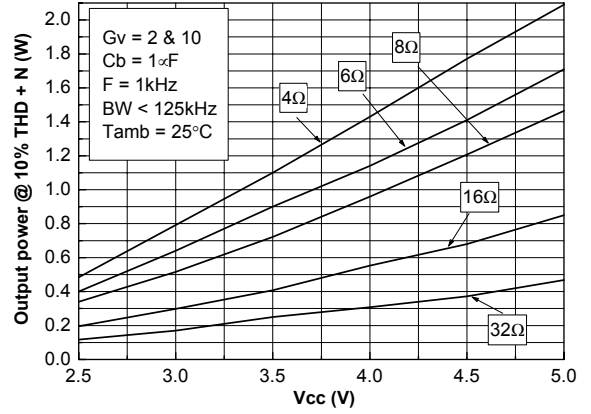
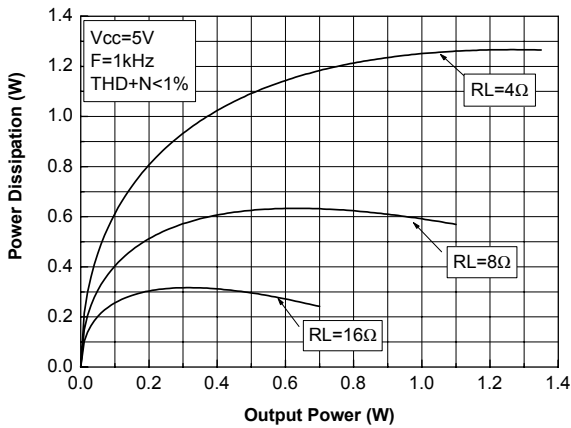
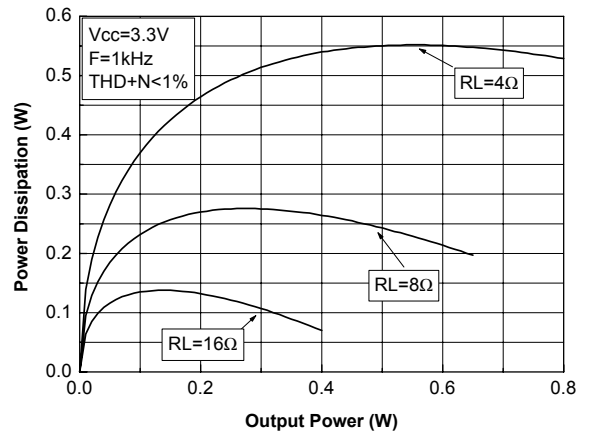
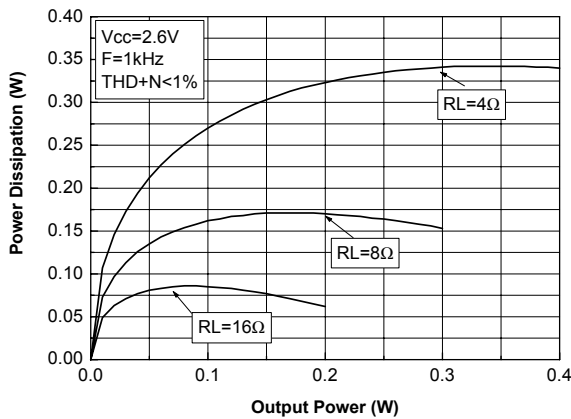
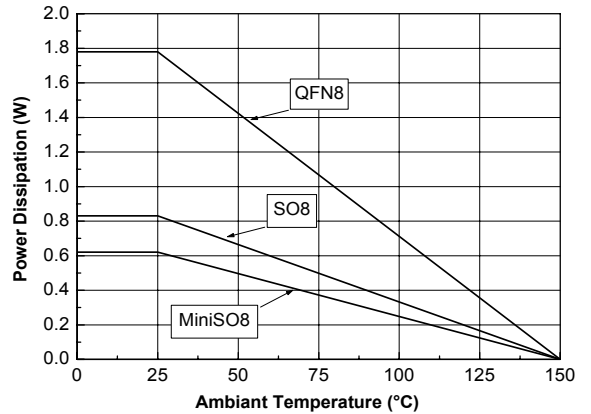
Figure 16. Pout @ THD + N = 1% vs supply voltage vs RL

Figure 17. Pout @ THD + N = 10% vs supply voltage vs RL

Figure 18. Power dissipation vs Pout Vcc=5 V

Figure 19. Power dissipation vs Pout Vcc=3.3 V

Figure 20. Power dissipation vs Pout Vcc=2.6 V

Figure 21. Power derating curves


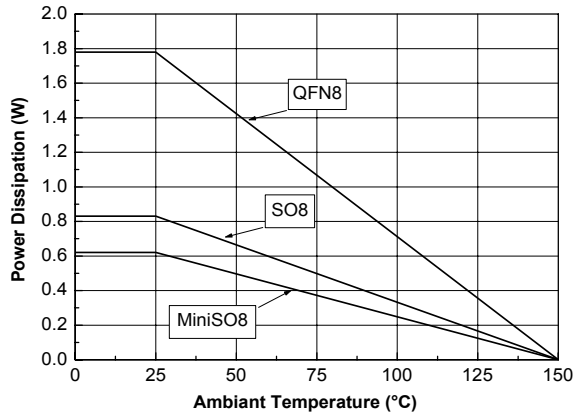
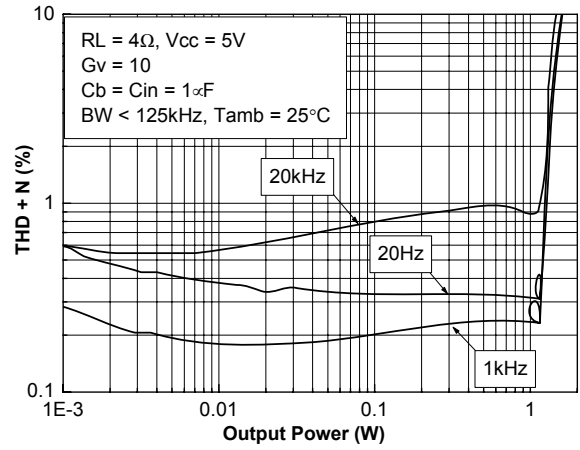
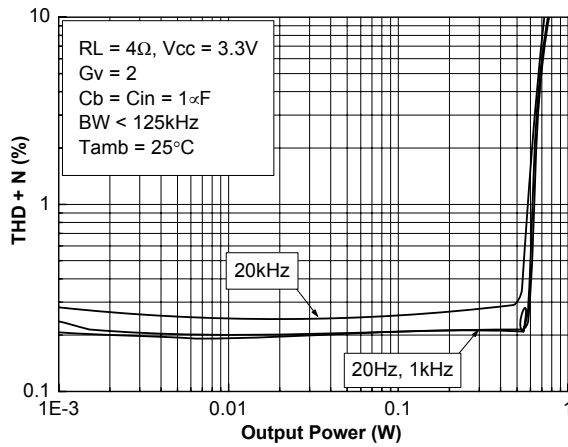
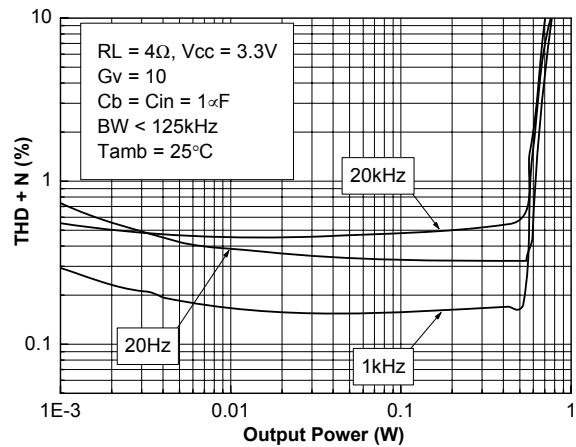
Figure 22. THD + N vs output power Gv=2, Vcc= 5 V

Figure 23. THD + N vs output power Gv=10, Vcc =5 V

Figure 24. THD + N vs output power Gv=2, Vcc = 3.3 V

Figure 25. THD + N vs output power Gv=10, Vcc = 3.3 V


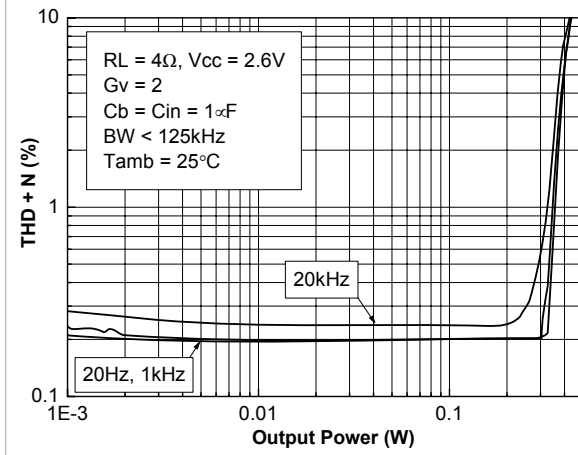
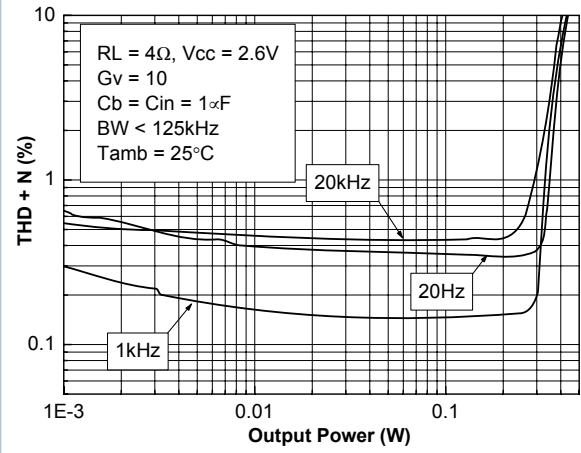
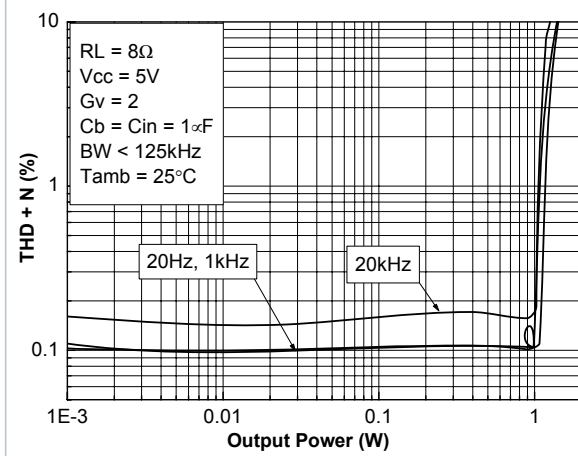
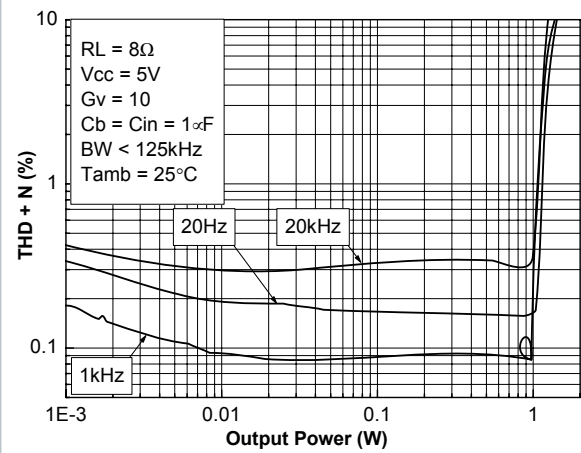
Figure 26. THD + N vs output power $G_v=2$, $V_{cc} = 2.6\text{ V}$

Figure 27. THD + N vs output power $G_v=10$, $V_{cc} = 2.6\text{ V}$

Figure 28. THD + N vs output power $G_v=2$, $V_{cc}= 5\text{ V}$, $RL=8\Omega$

Figure 29. THD + N vs output power $G_v=10$, $V_{cc} = 5\text{ V}$


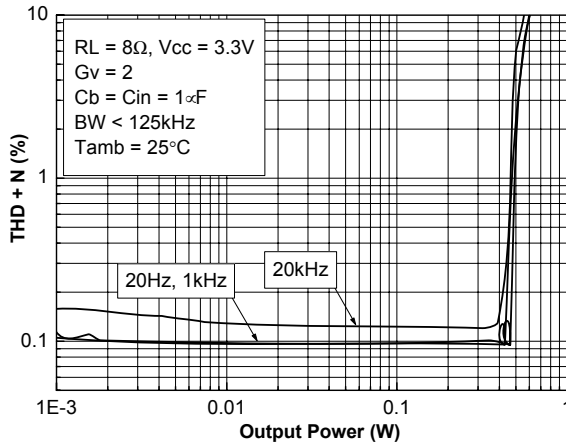
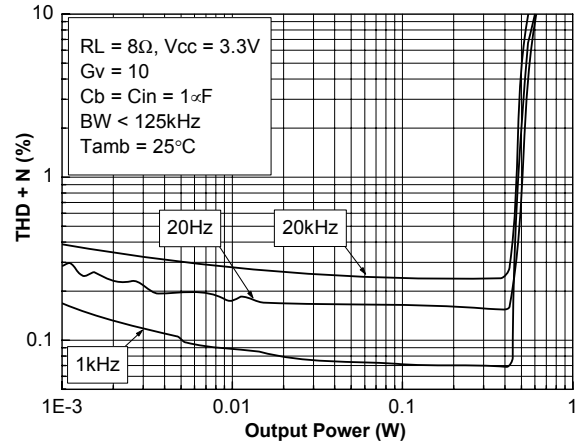
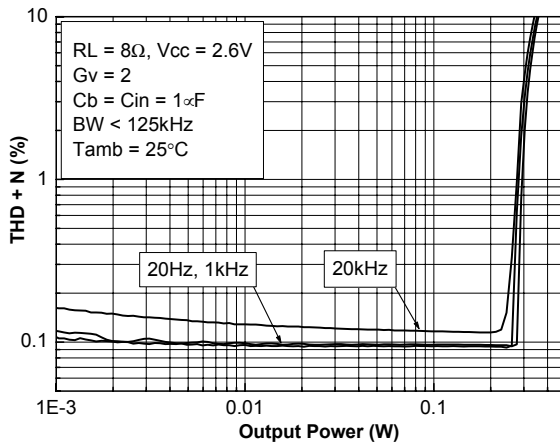
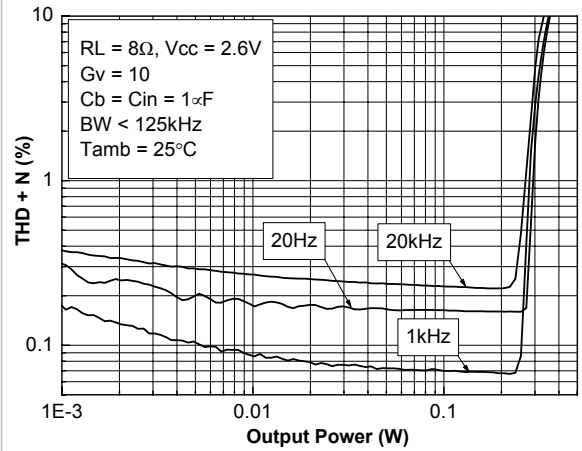
Figure 30. THD + N vs output power RL= 8 Ω

Figure 31. THD + N vs output power RL= 8 Ω , Vcc=3.3 V

Figure 32. THD + N vs output power RL= 8 Ω , Vcc=2.6 V

Figure 33. THD + N vs output power RL= 8 Ω , Gv=10


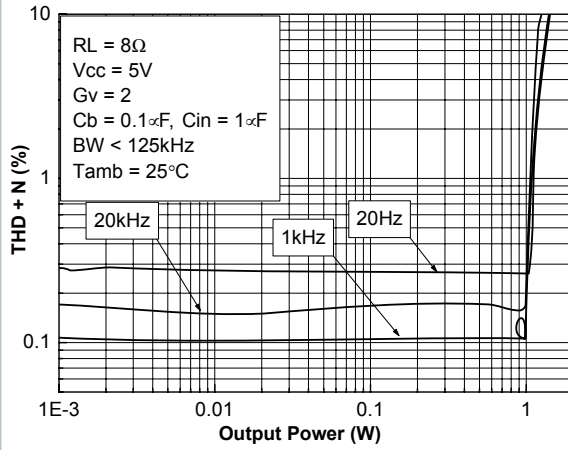
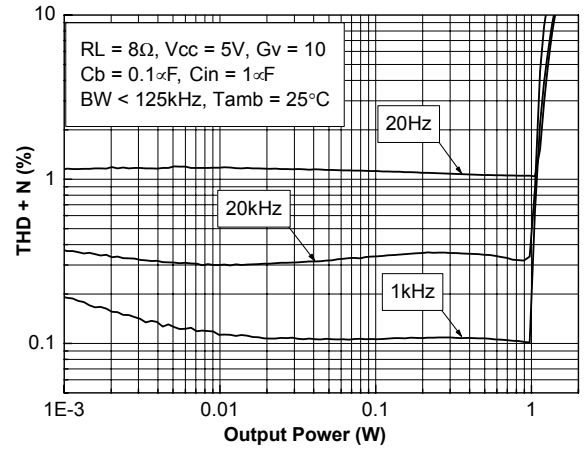
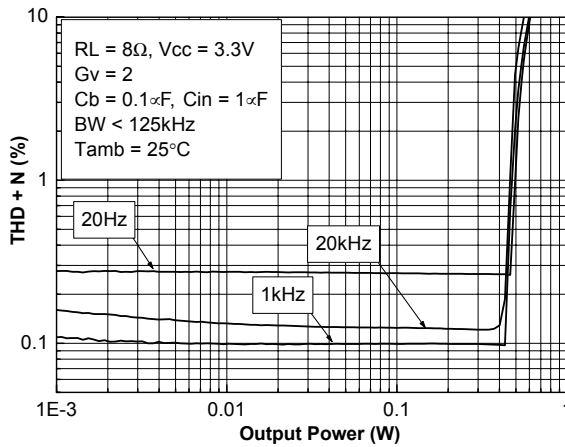
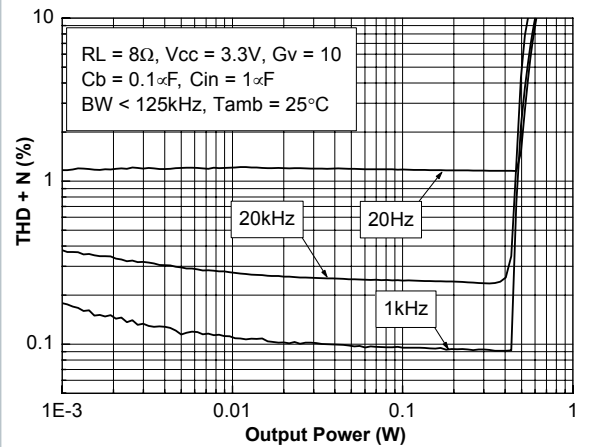
Figure 34. THD + N vs output power Gv=2, Vcc=5 V, Cb=0.1 μ F

Figure 35. THD + N vs output power Gv=10, Vcc = 5 V, Cb=0.1 μ F

Figure 36. THD + N vs output power Gv=2, Vcc = 3.3 V, Cb=0.1 μ F

Figure 37. THD + N vs output power Gv=10, Vcc=3.3 V, Cb=0.1 μ F


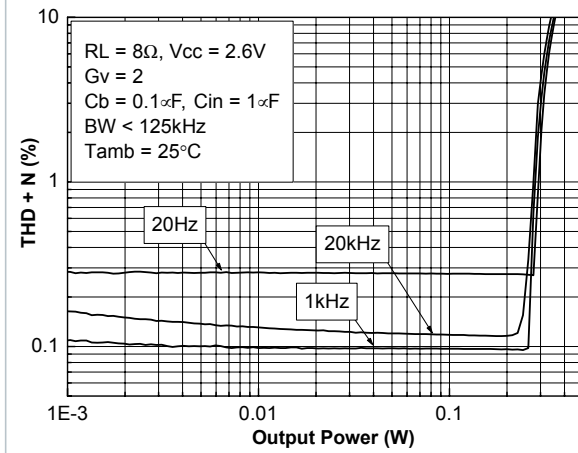
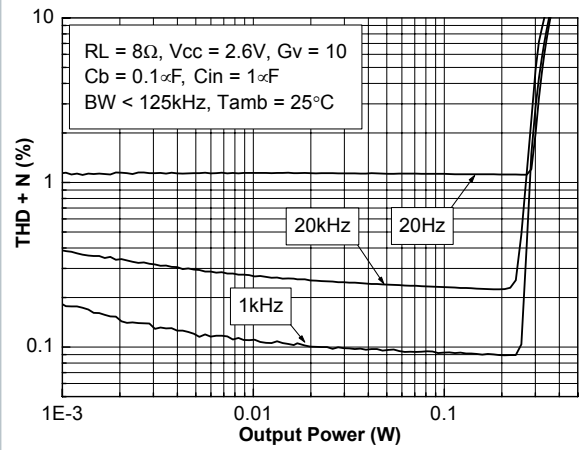
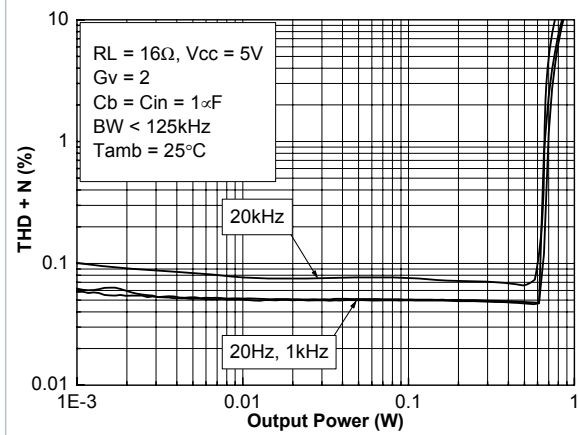
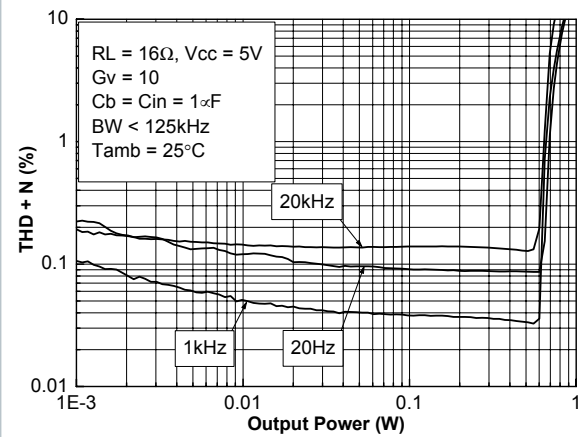
Figure 38. THD + N vs output power $G_v=2$, $V_{cc} = 2.6\text{ V}$, $C_b=0.1\ \mu\text{F}$

Figure 39. THD + N vs output power $G_v=10$, $V_{cc}=2.6\text{ V}$, $C_b=0.1\ \mu\text{F}$

Figure 40. THD + N vs output power $RL=16\ \Omega$ $V_{cc}=0.5\text{ V}$

Figure 41. THD + N vs output power $RL=16\ \Omega$ $G_v=10$


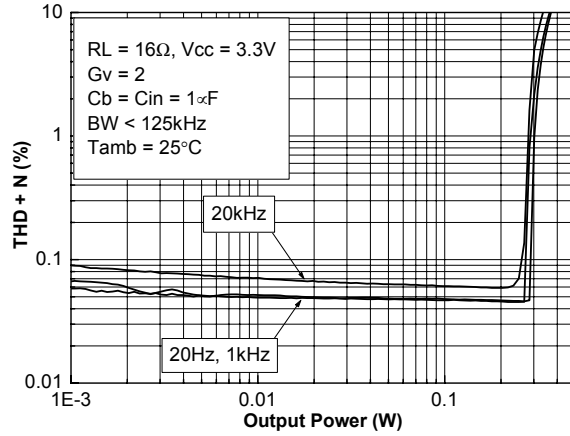
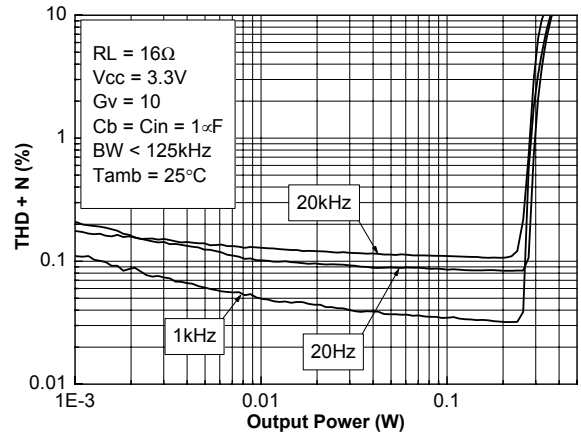
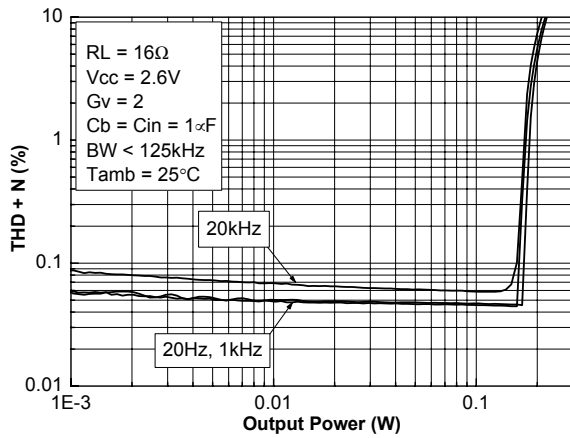
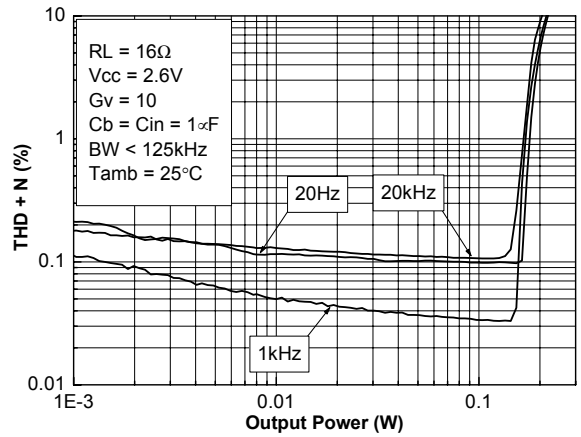
Figure 42. THD + N vs output power $R_L=16\ \Omega$, $G_v=2$

Figure 43. THD + N vs output power $R_L=16\ \Omega$, $G_v=10$, $V_{CC}=3.3\ \text{V}$

Figure 44. THD + N vs output power $R_L=16\ \Omega$, $V_{CC}=2.6\ \text{V}$

Figure 45. THD + N vs output power $R_L=16\ \Omega$, $V_{CC}=2.6\ \text{V}$, $G_v=10$


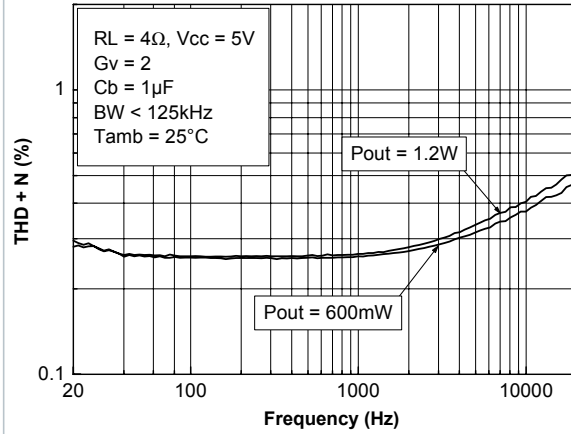
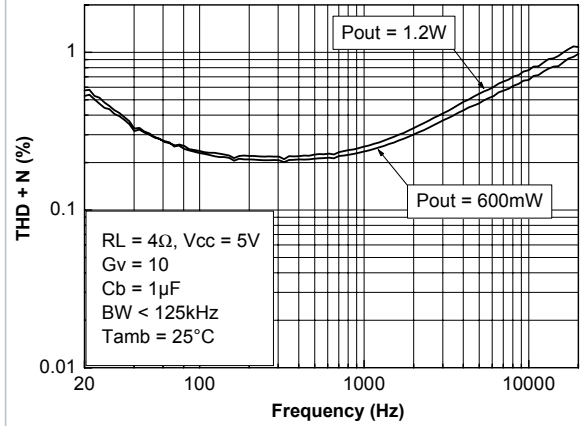
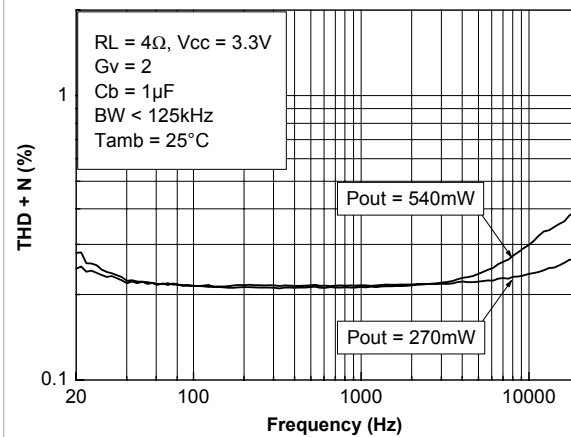
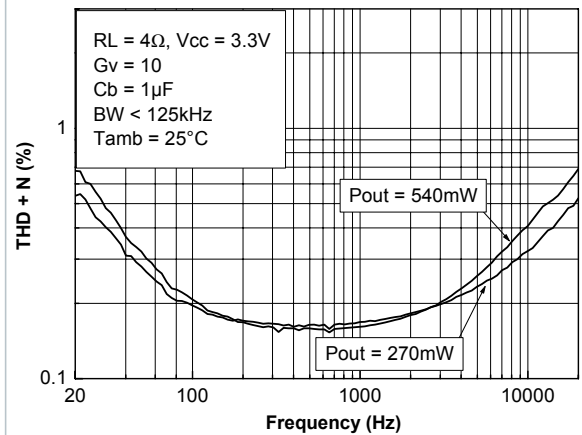
Figure 46. THD + N vs frequency

Figure 47. THD + N vs frequency, $V_{cc}=5V$

Figure 48. THD + N vs frequency, $V_{cc}=3.3V$

Figure 49. THD + N vs frequency, $G_v=10$


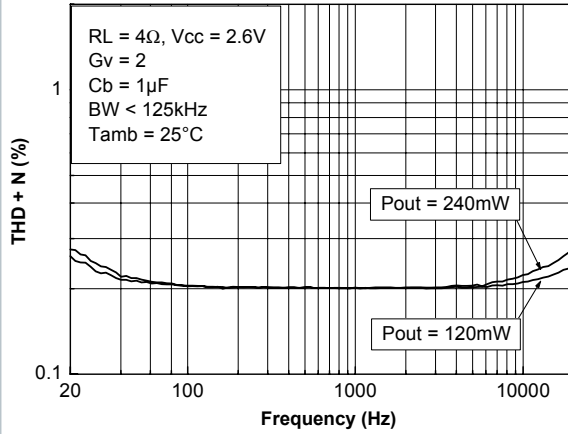
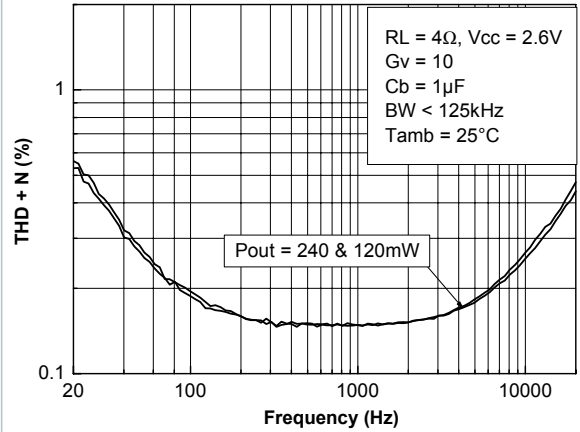
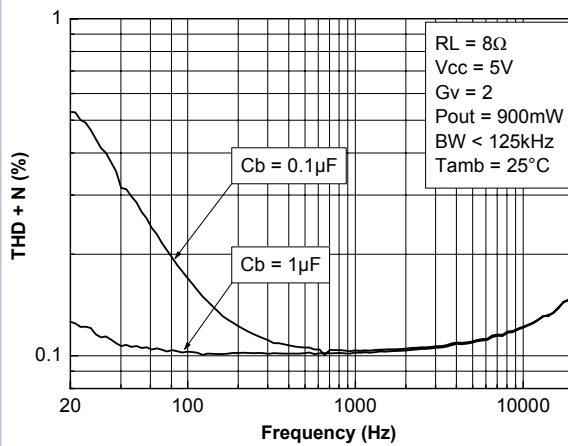
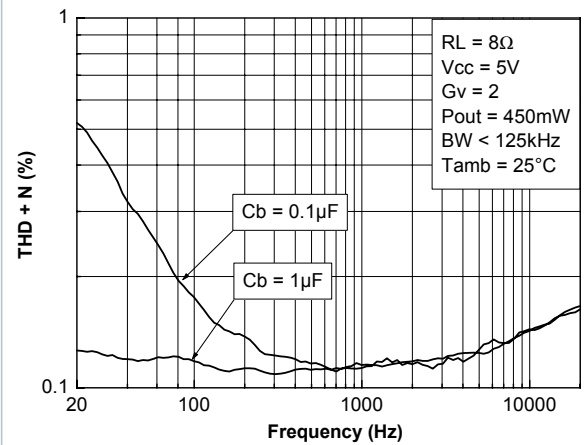
Figure 50. THD + N vs frequency, $V_{cc}=2.6\text{ V}$

Figure 51. THD + N vs frequency, $V_{cc}=2.6\text{ V}$, $RL = 4\ \Omega$

Figure 52. THD + N vs frequency, $V_{cc}=5\text{ V}$, $RL=8\ \Omega$

Figure 53. THD + N vs frequency, $P_{out}=450\text{ mW}$


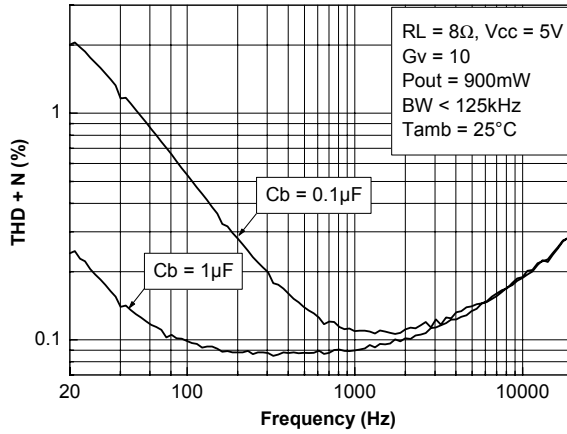
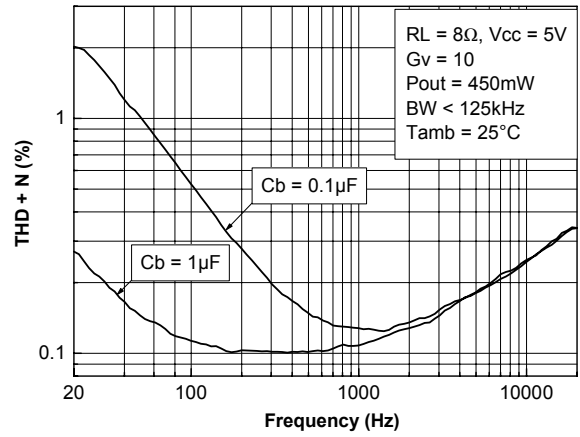
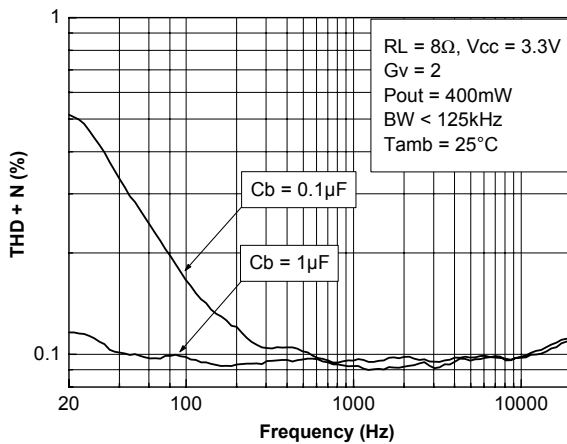
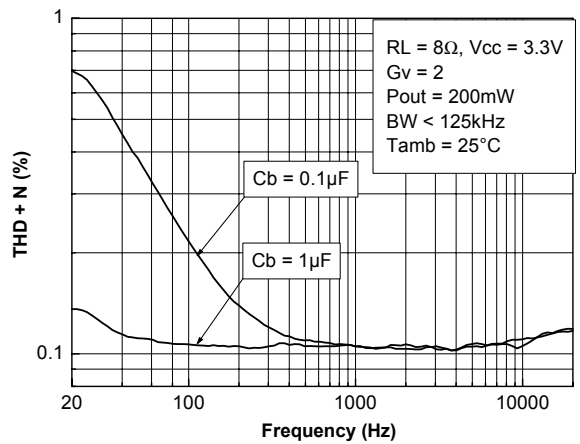
Figure 54. THD + N vs frequency, Pout=900 mW

Figure 55. THD + N vs frequency, Pout=450 mW, RL=8 Ω

Figure 56. THD + N vs frequency, Pout=400 mW

Figure 57. THD + N vs frequency, Pout=200 mW


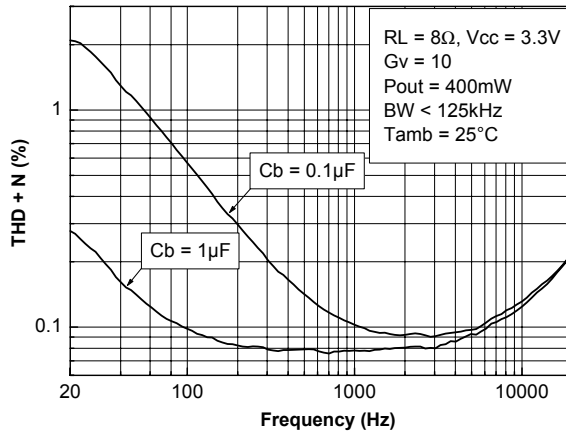
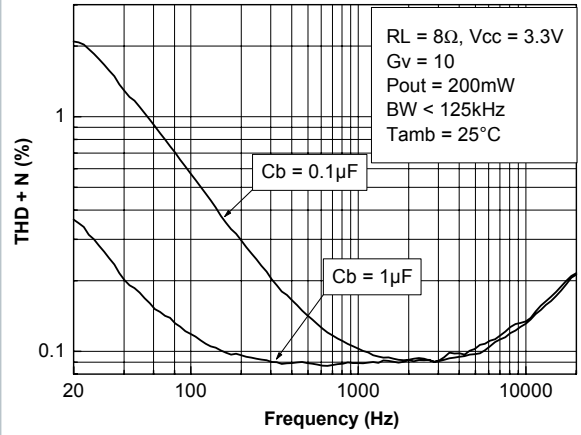
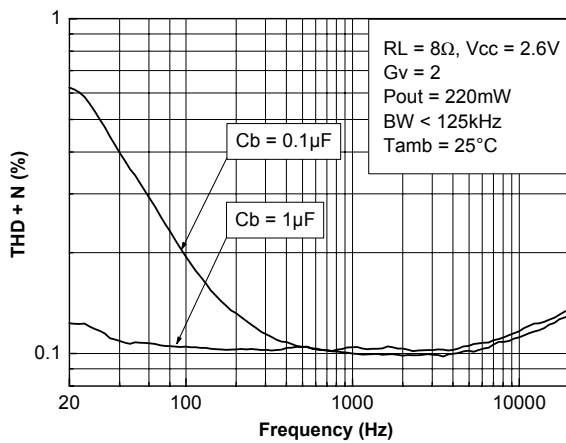
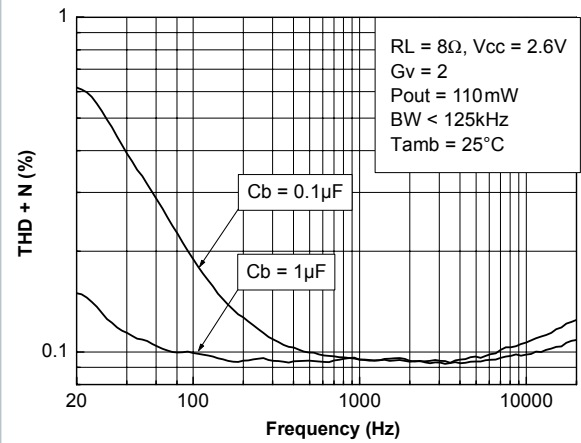
Figure 58. THD + N vs frequency, Pout=400 mW, Gv=010

Figure 59. THD + N vs frequency, Pout=200 mW

Figure 60. THD + N vs frequency, Pout=220 mW

Figure 61. THD + N vs frequency, Pout=110 mW


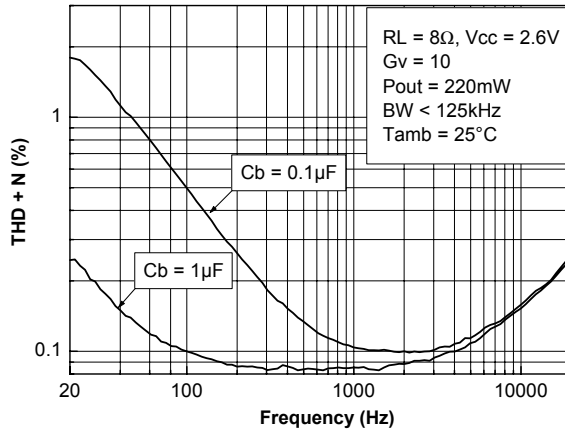
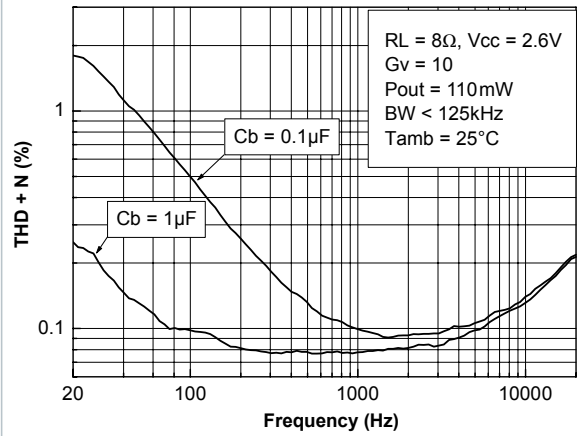
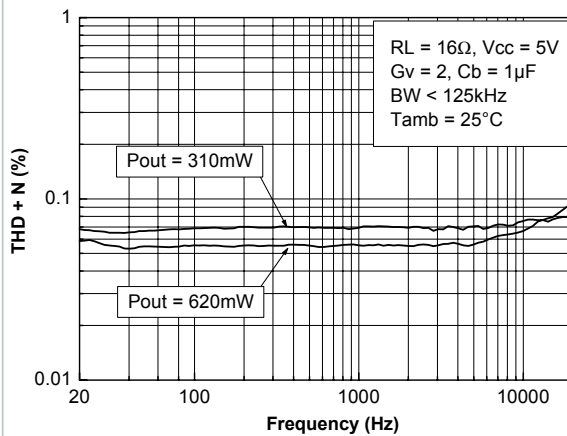
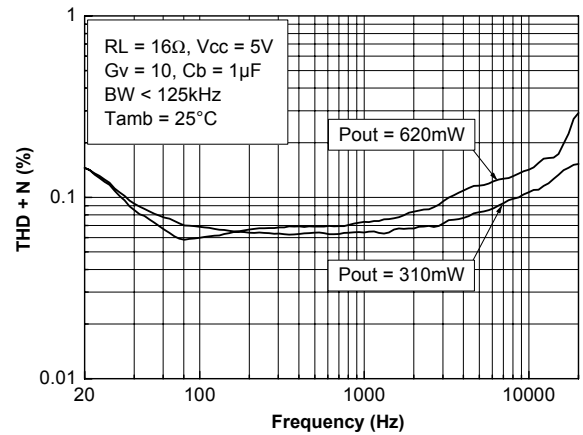
Figure 62. THD + N vs frequency, Pout=220 mW, Vcc= 2.6 V

Figure 63. THD + N vs frequency, Pout=110 mW, Vcc= 2.6 V

Figure 64. THD + N vs frequency, RL=16 Ω

Figure 65. THD + N vs frequency, RL=16 Ω , Gv=10


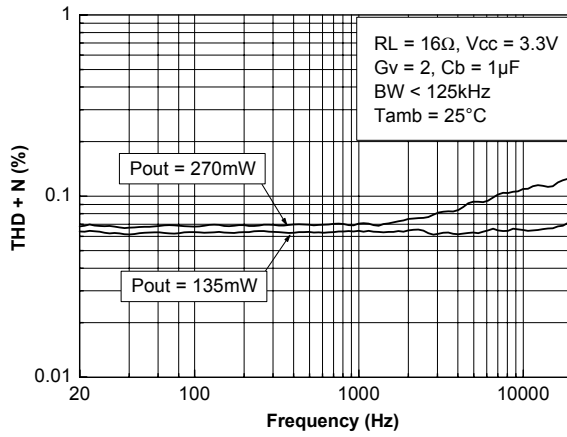
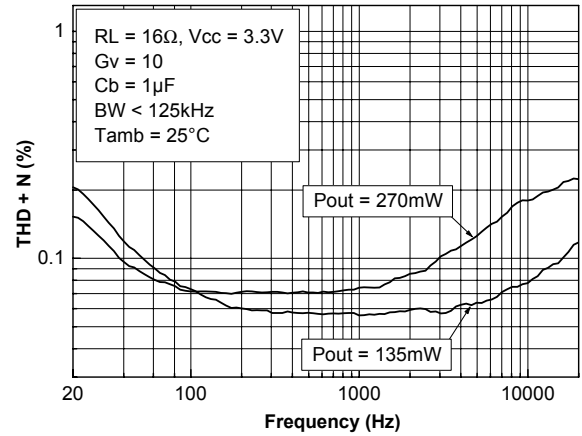
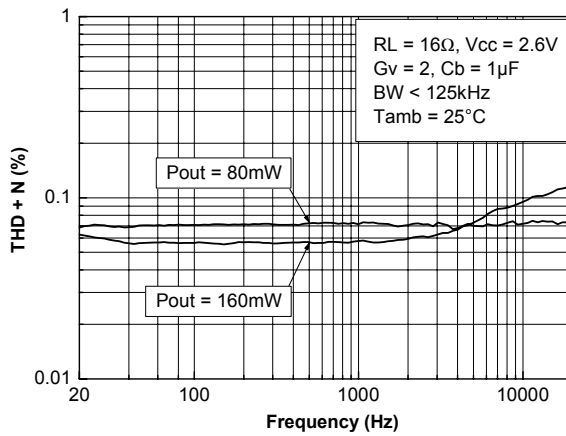
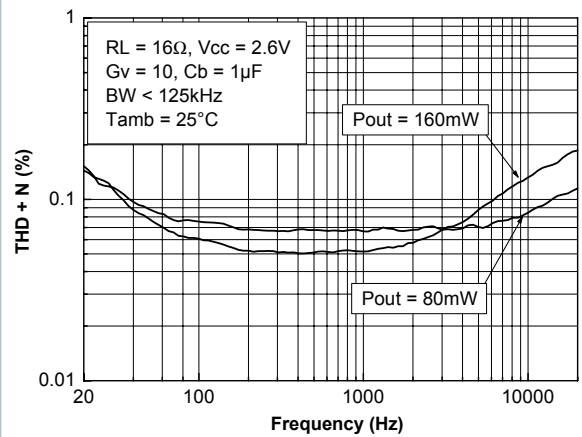
Figure 66. THD + N vs frequency, $RL=16\ \Omega$, $Gv=2$

Figure 67. THD + N vs frequency, $RL=16\ \Omega$, $Gv=10$, $Vcc=3.3\ V$

Figure 68. THD + N vs frequency, $RL=16\ \Omega$, $Gv=2$, $Vcc=2.6\ V$

Figure 69. THD + N vs frequency, $RL=16\ \Omega$, $Gv=10$, $Pout=160\ mW$


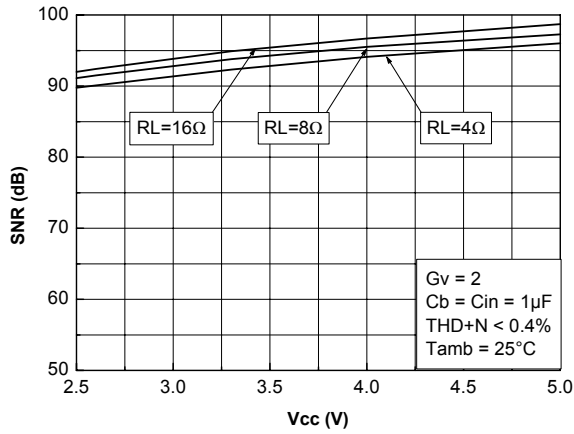
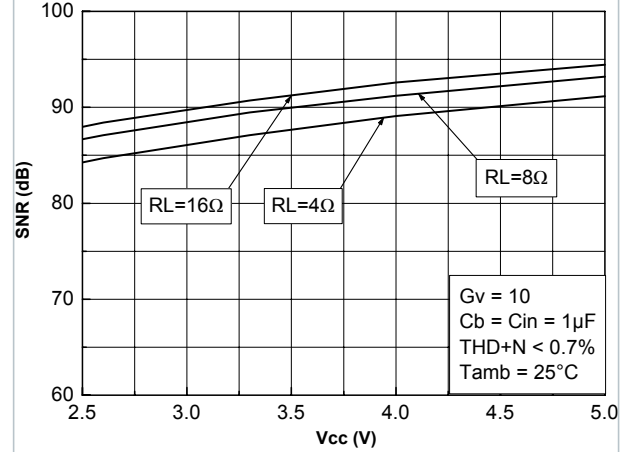
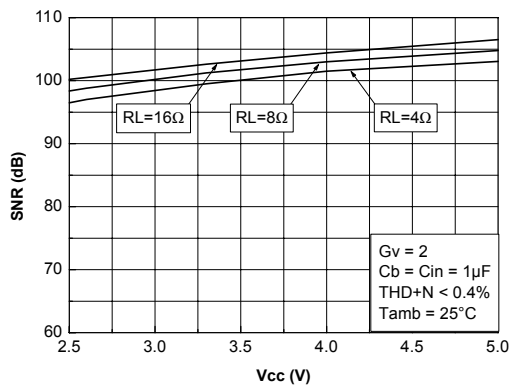
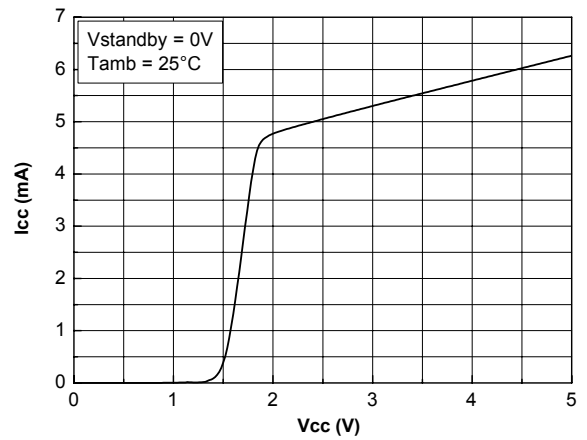
Figure 70. Signal-to-noise ratio vs power supply with unweighted filter (20 Hz to 20 kHz)

Figure 71. Signal-to-noise ratio vs power supply with weighted filter type A

Figure 72. Signal-to-noise ratio vs power supply with weighted filter type A Gv=2

Figure 73. Current consumption vs power supply voltage


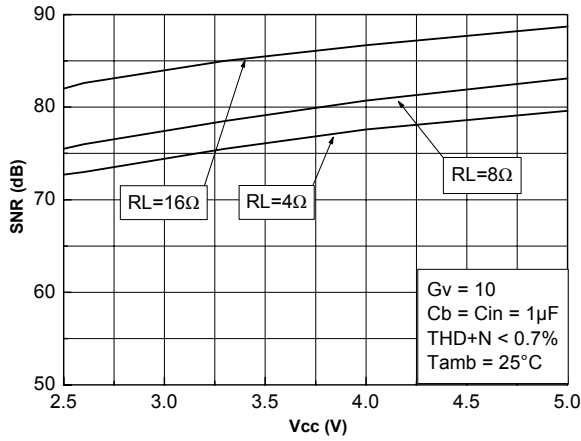
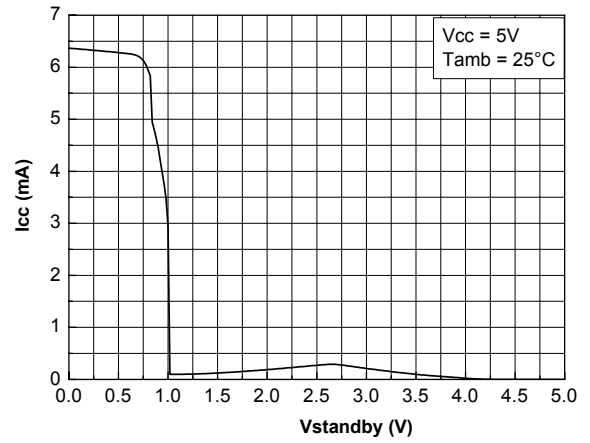
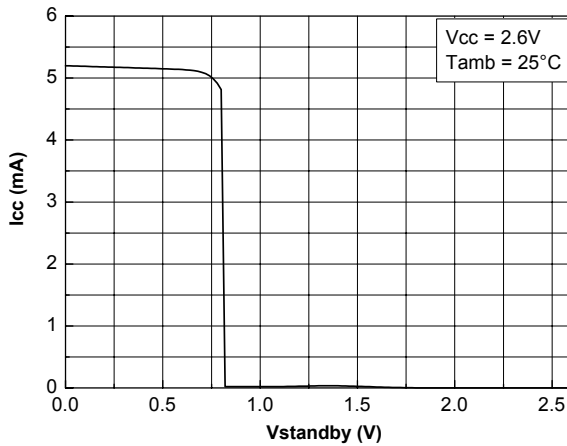
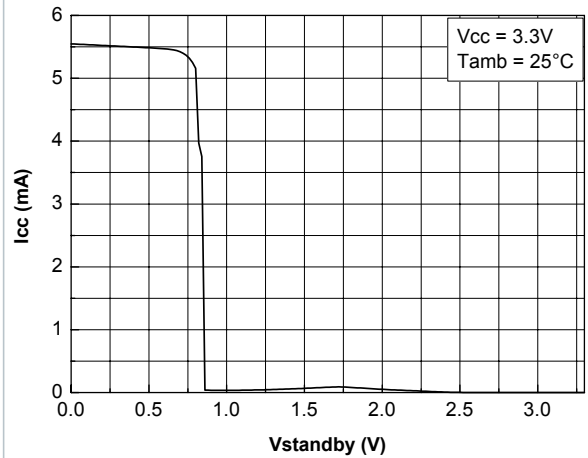
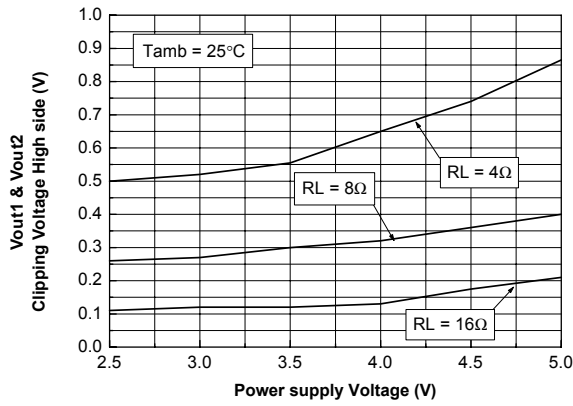
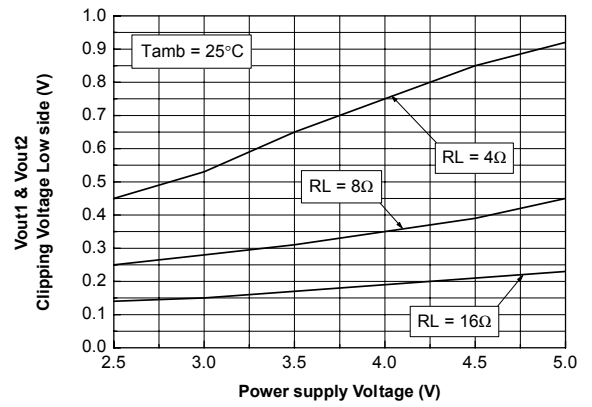
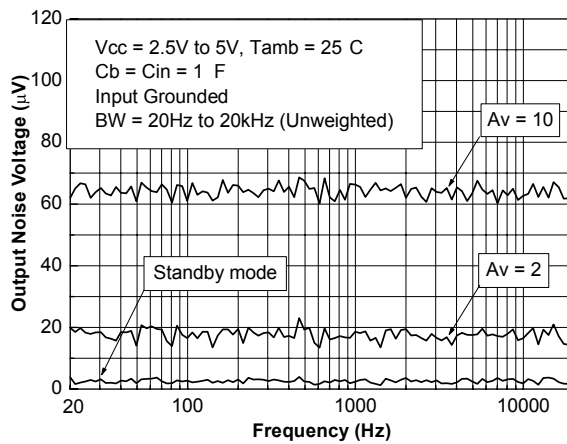
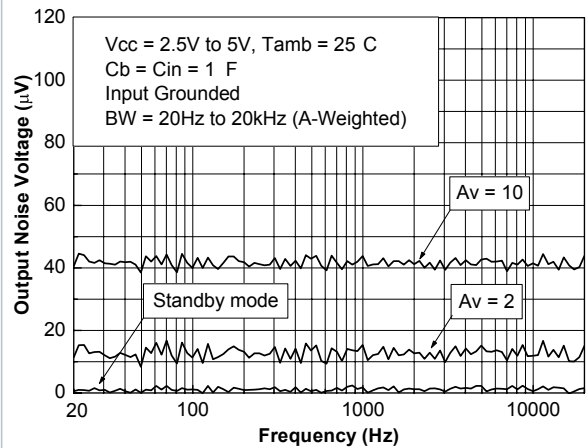
Figure 74. Signal-to-noise ratio vs power supply with unweighted filter (20 Hz to 20 kHz) $G_v=10$

Figure 75. Current consumption vs standby voltage @ $V_{cc} = 5 V$

Figure 76. Current consumption vs standby voltage @ $V_{cc} = 2.6 V$

Figure 77. Current consumption vs standby voltage @ $V_{cc} = 3.3 V$


Figure 78. Clipping voltage vs power supply voltage and load resistor

Figure 79. Clipping voltage low-side vs power supply voltage and load resistor

Figure 80. Vout1+Vout2 unweighted noise floor

Figure 81. Vout1+Vout2 A-weighted noise floor


5 Application information

Figure 82. Demoboard schematic

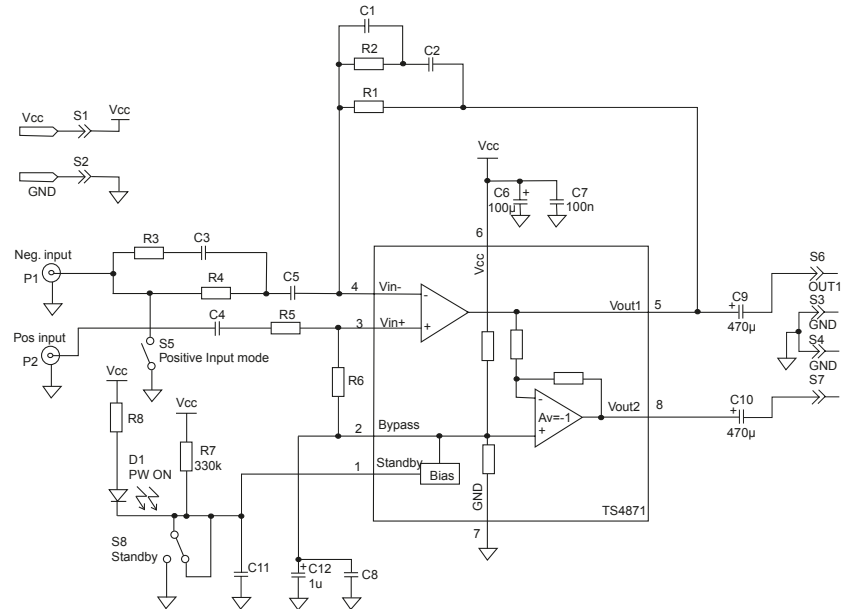


Figure 83. SO8 & MiniSO8 demoboard components side

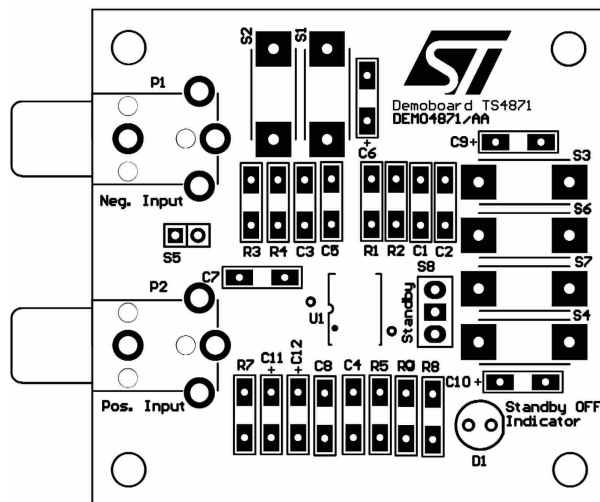


Figure 84. SO8 and MiniSO8 demoboard top solder layer

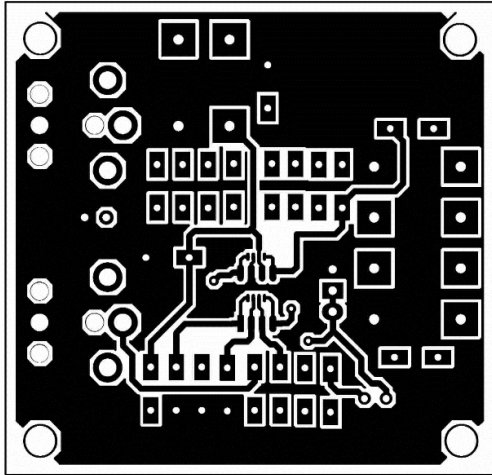
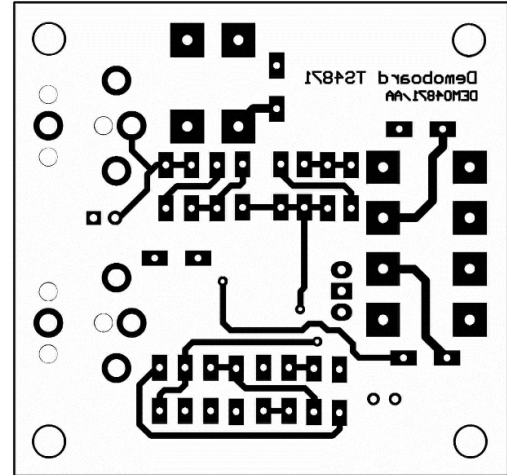


Figure 85. SO8 and MiniSO8 demoboard bottom solder layer



5.1 BTL configuration principle

The TS4871 is a monolithic power amplifier with a BTL output type. BTL (bridge tied load) means that each end of the load is connected to two single ended output amplifiers. Thus, we have:

Single ended output 1 = $V_{out1} = V_{out}$ (V)

Single ended output 2 = $V_{out2} = -V_{out}$ (V)

And $V_{out1} - V_{out2} = 2V_{out}$ (V)

The output power is:

$$P_{out} = \frac{(2V_{out_{RMS}})^2}{R_L} (W) \quad (1)$$

For the same power supply voltage, the output power in BTL configuration is four times higher than the output power in single ended configuration.

5.2 Gain In typical application schematic

In flat region (no effect of C_{in}), the output voltage of the first stage is:

$$V_{out1} = -V_{in} \frac{R_{feed}}{R_{in}} (V)$$

For the second stage : $V_{out2} = -V_{out1}$ (V)

The differential output voltage is:

$$V_{out2} - V_{out1} = 2V_{in} \frac{R_{feed}}{R_{in}} (V)$$

The differential gain named gain (G_v) for more convenient usage is:

$$G_v = \frac{V_{out2} - V_{out1}}{V_{in}} = 2 \frac{R_{feed}}{R_{in}}$$

Remark : V_{out2} is in phase with V_{in} and V_{out1} is 180 phased with V_{in} . It means that the positive terminal of the loud speaker should be connected to V_{out2} and the negative to V_{out1} .

5.3 Low and high frequency response

In low frequency region, the effect of C_{in} starts. C_{in} with R_{in} forms a high pass filter with a -3 dB cut-off frequency

$$F_{CL} = \frac{1}{2\pi R_{in} C_{in}} (\text{Hz})$$

In high frequency region, you can limit the bandwidth by adding a capacitor (C_{feed}) in parallel on R_{feed} . Its form a low pass filter with a -3 dB cut-off frequency.

$$F_{CH} = \frac{1}{2\pi R_{feed} C_{feed}} (\text{Hz})$$

5.4 Power dissipation and efficiency

Hypothesis:

- Voltage and current in the load are sinusoidal (V_{out} and I_{out})
- Supply voltage is a pure DC source (V_{cc})

Regarding the load we have:

$$V_{OUT} = V_{PEAK} \sin \omega t(t)$$

and

$$I_{OUT} = \frac{V_{OUT}}{R_L} (A)$$

$$P_{OUT} = \frac{V_{PEAK}^2}{2R_L} (W)$$

Then, the average current delivered by the supply voltage is:

$$I_{CCAVG} = 2 \frac{V_{PEAK}}{\pi R_L} (A)$$

The power delivered by the supply voltage is $P_{supply} = V_{cc} I_{CCAVG}$ (W)

Then, the power dissipated by the amplifier is $P_{diss} = P_{supply} - P_{out}$ (W)

$$P_{diss} = \frac{2\sqrt{2}V_{cc}}{\pi\sqrt{R_L}} \sqrt{P_{OUT}} - P_{OUT} (W)$$

and the maximum value is obtained when:

$$\frac{\partial P_{diss}}{\partial P_{OUT}} = 0$$

and its value is:

$$P_{dissmax} = \frac{2V_{CC}^2}{\pi^2 R_L} (W)$$

Remark : This maximum value is only depending on power supply voltage and load values.

The efficiency is the ratio between the output power and the power supply

$$\eta = \frac{P_{OUT}}{P_{supply}} = \frac{\pi V_{PEAK}}{4V_{CC}}$$

The maximum theoretical value is reached when

$V_{peak} = V_{cc}$, so

$$\frac{\pi}{4} = 78.5\%$$

5.5 Decoupling of the circuit

Two capacitors are needed to bypass properly the TS4871, a power supply bypass capacitor C_s and a bias voltage bypass capacitor C_b .

C_s has especially an influence on the THD+N in high frequency (above 7 kHz) and indirectly on the power supply disturbances.

With 100 μF , you can expect similar THD+N performances like shown in the datasheet.

If C_s is lower than 100 μF , in high frequency increases, THD+N and disturbances on the power supply rail are less filtered.

To the contrary, if C_s is higher than 100 μF , those disturbances on the power supply rail are more filtered.

C_b has an influence on THD+N in lower frequency, but its function is critical on the final result of PSRR with input grounded in lower frequency.

If C_b is lower than 1 μF , THD+N increase in lower frequency (see THD+N vs frequency curves) and the PSRR worsens up.

If C_b is higher than 1 μF , the benefit on THD+N in lower frequency is small but the benefit on PSRR is substantial (see PSRR vs. C_b curve: fig.12).

Note that C_{in} has a non-negligible effect on PSRR in lower frequency. Lower is its value, higher is the PSRR (see fig. 13).

5.6 Pop and Click performance

Pop and click performance is intimately linked to the size of the input capacitor C_{in} and the bias voltage bypass capacitor C_b .

Size of C_{in} is due to the lower cut-off frequency and PSRR value requested. Size of C_b is due to THD+N and PSRR requested always in lower frequency.

Moreover, C_b determines the speed that the amplifier turns ON. The slower the speed is, the softer the turn ON noise is.

The charge time of C_b is directly proportional to the internal generator resistance 50 $\text{k}\Omega$.

Then, the charge time constant for C_b is

$$\tau_b = 50 \text{ k}\Omega \times C_b \text{ (s)}$$

As C_b is directly connected to the non-inverting input (pin 2 and 3) and if we want to minimize, in amplitude and duration, the output spike on V_{out1} (pin 5), C_{in} must be charged faster than C_b . The charge time constant of C_{in} is

$$\tau_{in} = (R_{in} + R_{feed}) \times C_{in} \text{ (s)}$$

Thus we have the relation

$$\tau_{in} \ll \tau_b \text{ (s)}$$

The respect of this relation allows the pop and click noise to be minimized.

Remark : Minimize C_{in} and C_b has a benefit on pop and click phenomena but also on cost and size of the application.

Example : your target for the -3 dB cut off frequency is 100 Hz. With $R_{in} = R_{feed} = 22 \text{ k}\Omega$, $C_{in} = 72 \text{ nF}$ (in fact 82 nF or 100 nF).

With $C_b = 1 \mu\text{F}$, if you choose the one of the latest two values of C_{in} , the pop and click phenomena at power supply ON or standby function ON/OFF will be very small

$$50 \text{ k}\Omega \times 1 \mu\text{F} \gg 44 \text{ k}\Omega \times 100 \text{ nF} \quad (50 \text{ ms} \gg 4.4 \text{ ms}).$$

Increasing C_{in} value increases the pop and click phenomena to an unpleasant sound at power supply ON and standby function ON/OFF.

Why C_s is not important in pop and click consideration ?

Hypothesis :

$$C_s = 100 \mu\text{F}$$

$$\text{Supply voltage} = 5 \text{ V}$$

$$\text{Supply voltage internal resistor} = 0.1 \Omega$$

$$\text{Supply current of the amplifier } I_{cc} = 6 \text{ mA}$$

At power ON of the supply, the supply capacitor is charged through the internal power supply resistor. So, to reach 5 V you need about five to ten times the charging time constant of C_s ($\tau_s = 0.1 \times C_s$ (s)).

Then, this time equal 50 μs to 100 μs $\ll \tau_b$ in the majority of application.

At power OFF of the supply, C_s is discharged by a constant current I_{cc} . The discharge time from 5 V to 0 V of C_s is:

$$t_{DischC_s} = \frac{5C_s}{I_{cc}} = 83 \text{ ms}$$

Now, we must consider the discharge time of C_b .

At power OFF or standby ON, Cb is discharged by a 100 kΩ resistor. So the discharge time is about

$$t_{bDisch} \approx 3 \times C_b \times 100 \text{ k}\Omega \text{ (s)}$$

In the majority of application, Cb = 1 μF, then

$$t_{bDisch} \approx 300 \text{ ms} \gg \tau_{dischC_b}$$

5.7 Power amplifier design examples

Given :

Load impedance : 8 Ω

Output power @ 1% THD+N : 0.5 W

Input impedance : 10 kΩ min.

Input voltage peak to peak : 1 Vpp

Bandwidth frequency : 20 Hz to 20 kHz (0, -3 dB)

Ambient temperature max = 50 °C

SO8 package

First of all, we must calculate the minimum power supply voltage to obtain 0.5 W into 8 Ω. With curves in fig. 15, we can read 3.5 V. Thus, the power supply voltage value min. is 3.5 V.

Following the maximum power dissipation equation

$$P_{dissmax} = \frac{2V_{CC}^2}{\pi^2 R_L} = \left(W \right)$$

with 3.5 V we have $P_{dissmax} = 0.31 \text{ W}$

Refer to power derating curves (fig. 20), with 0.31 W the maximum ambient temperature is 100 °C. This last value could be higher if you follow the example layout shown on the demoboard (better dissipation).

The gain of the amplifier in flat region is:

$$G_V = \frac{V_{OUTPP}}{V_{INPP}} = \frac{2\sqrt{2R_L P_{OUT}}}{V_{INPP}} = 5.65$$

We have $R_{in} > 10 \text{ k}\Omega$. Let's take $R_{in} = 10 \text{ k}\Omega$, then $R_{feed} = 28.25 \text{ k}\Omega$. We could use for $R_{feed} = 30 \text{ k}\Omega$ in normalized value and the gain is $G_v = 6$.

In lower frequency we want 20 Hz (-3dB cut-off frequency). Then:

So, we could use for C_{in} a 1 μF capacitor value

$$C_{IN} = \frac{1}{2\pi R_{in} F_{CL}} = 795 \text{ nF}$$

which gives 16 Hz.

In higher frequency we want 20 kHz (-3dB cut off frequency). The gain bandwidth product of the TS4871 is 2 MHz typical and does not change when the amplifier delivers power into the load.

The first amplifier has a gain of:

$$\frac{R_{feed}}{R_{in}} = 3$$

and the theoretical value of the -3 dB cut-off higher frequency is $2 \text{ MHz}/3 = 660 \text{ kHz}$.

We can keep this value or limit the bandwidth by adding a capacitor C_{feed} , in parallel on R_{feed} .

Then:

$$C_{FEED} = \frac{1}{2\pi R_{FEED} F_{CH}} = 265 \text{ pF}$$

So, we could use for C_{feed} a 220 pF capacitor value that gives 24 kHz.

Now, we can calculate the value of C_b with the formula $\tau_b = 50 \text{ k}\Omega \times C_b \gg \tau_{in} = (R_{in} + R_{feed}) \times C_{in}$ which permits to reduce the pop and click effects.

Then $C_b \gg 0.8 \mu\text{F}$.

We can choose for C_b a normalized value of 2.2 μF that gives good results in THD+N and PSRR.

In the following tables, you could find three another examples with values required for the demoboard.

Remark : components with (*) marking are optional.

5.8 Application n°1 : 20 Hz to 20 kHz bandwidth and 6 dB gain BTL power amplifier

Table 7. Components

| Designator | Part type |
|----------------|------------------------------------|
| R1 | 22 k / 0.125 W |
| R4 | 22 k / 0.125 W |
| R6 | Short-circuit |
| R7 | 330 k / 0.125 W |
| R8* | (Vcc-Vf_led) / If_led |
| C5 | 470 nF |
| C6 | 100 µF |
| C7 | 100 nF |
| C9 | Short-circuit |
| C10 | Short-circuit |
| C12 | 1 µF |
| S1, S2, S6, S7 | 2 mm insulated plug 10.16 mm pitch |
| S8 | 3 pt connector 2.54 mm pitch |
| P1 | PCB phono Jack |
| D1* | Led 3 mm |
| U1 | TS4871ID or TS4871IS |

5.9 Application n°2 : 20 Hz to 20 kHz bandwidth and 20 dB gain BTL power amplifier

Table 8. Components

| Designator | Part type |
|----------------|--------------------------------------|
| R1 | 110 k / 0.125 W |
| R4 | 22 k / 0.125 W |
| R6 | Short-circuit |
| R7 | 330 k / 0.125 W |
| R8* | $(V_{cc} - V_{f_led}) / I_{f_led}$ |
| C5 | 470 nF |
| C6 | 100 μ F |
| C7 | 100 nF |
| C9 | Short-circuit |
| C10 | Short-circuit |
| C12 | 1 μ F |
| S1, S2, S6, S7 | 2 mm insulated plug 10.16 mm pitch |
| S8 | 3 pt connector 2.54 mm pitch |
| P1 | PCB phono Jack |
| D1* | Led 3 mm |
| U1 | TS4871ID or TS4871IS |

5.10 Application n° 3: 50 Hz to 10 kHz bandwidth and 10 dB gain BTL power amplifier

Table 9. Components

| Designator | Part type |
|----------------|------------------------------------|
| R1 | 33 k / 0.125 W |
| R2 | Short-circuit |
| R4 | 22 k / 0.125 W |
| R6 | Short-circuit |
| R7 | 330 k / 0.125 W |
| R8* | $(V_{cc}-V_{f_led}) / I_{f_led}$ |
| C2 | 470 pF |
| C5 | 150 nF |
| C6 | 100 μ F |
| C7 | 100 nF |
| C9 | Short-circuit |
| C10 | Short-circuit |
| C12 | 1 μ F |
| S1, S2, S6, S7 | 2 mm insulated plug 10.16 mm pitch |
| S8 | 3 pts connector 2.54 mm pitch |
| P1 | PCB phono Jack |
| D1* | Led 3 mm |
| U1 | TS4871ID or TS4871IS |

5.11 Application n°4 : Differential inputs BTL power amplifier

In this configuration, we need to place these components : R1, R4, R5, R6, R7, C4, C5, C12.

We have also : R4 = R5, R1 = R6, C4 = C5.

The gain of the amplifier is:

$$G_{VDIFF} = 2 \frac{R1}{R4}$$

For Vcc = 5 V, a 20 Hz to 20 kHz bandwidth and 20 dB gain BTL power amplifier you could follow the bill of material below.

Table 10. Components

| Designator | Part type |
|----------------|------------------------------------|
| R1 | 110 k / 0.125 W |
| R4 | 22 k / 0.125 W |
| R5 | 22 k / 0.125 W |
| R6 | 110 k / 0.125 W |
| R7 | 330 k / 0.125 W |
| R8* | (Vcc-Vf_led) / If_led |
| C4 | 470 nF |
| C5 | 470 nF |
| C6 | 100 µF |
| C7 | 100 nF |
| C9 | Short-circuit |
| C10 | Short-circuit |
| C12 | 1 µF |
| D1* | Led 3 mm |
| S1, S2, S6, S7 | 2 mm insulated plug 10.16 mm pitch |
| S8 | 3 pts connector 2.54 mm pitch |
| P1, P2 | PCB phono Jack |
| U1 | TS4871ID or TS4871IS |

5.12 Note on how to use the PSRR curves

We have finished a design and we have chosen the components values

- Rin=Rfeed=22 kΩ
- Cin=100 nF
- Cb=1 µF

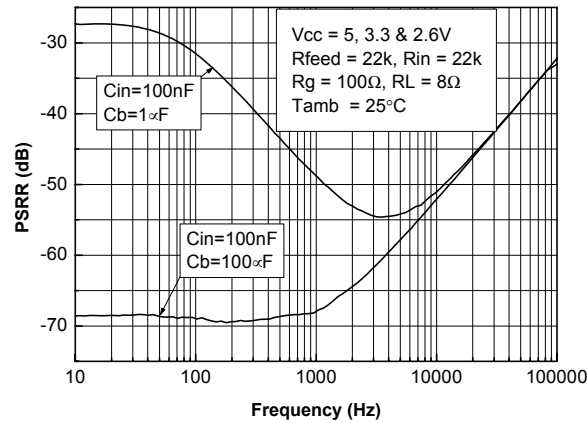
Now, on fig. 13, we can see the PSRR (input grounded) vs. frequency curves. At 217 Hz we have a PSRR value of -36 dB.

In reality we want a value about -70 dB. So, we need a gain of 34 dB.

Now, on fig. 12 we can see the effect of Cb on the PSRR (input grounded) vs. frequency. With Cb=100 µF, we can reach the -70 dB value.

The process to obtain the final curve (Cb=100 µF, Cin=100 nF, Rin=Rfeed=22 kΩ) is a simple transfer point by point on each frequency of the curve on fig. 13 to the curve on fig. 12. The measurement result is shown on the next figure.

Figure 86. PSRR changes with Cb



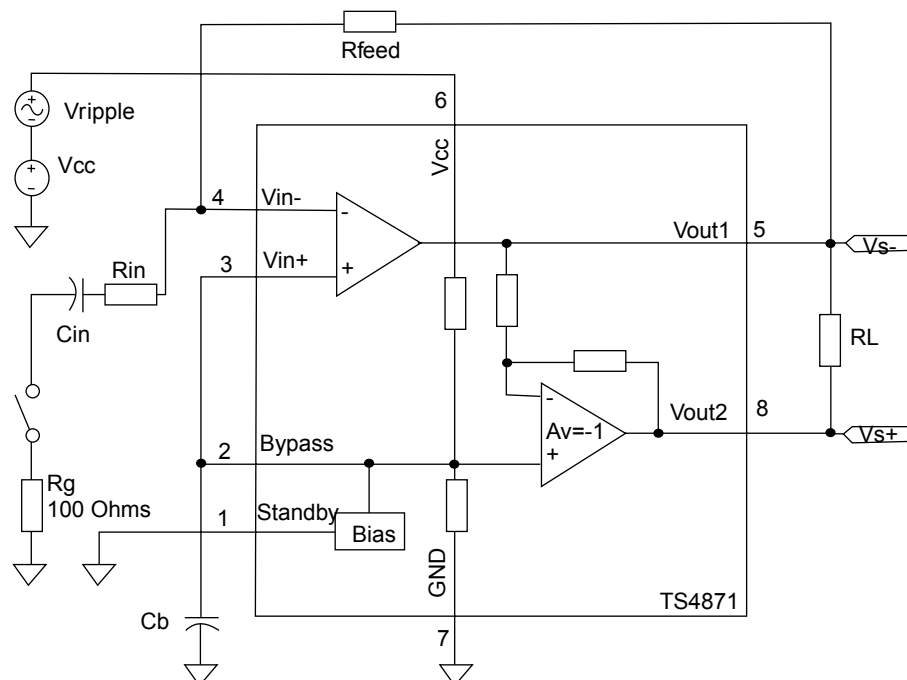
What is the PSRR?

The PSRR is the power supply rejection ratio. It is a kind of SVR in a determined frequency range.

The PSRR of a device, is the ratio between a power supply disturbance and the result on the output. We can say that the PSRR is the ability of a device to minimize the impact of power supply disturbances to the output.

How do we measure the PSRR?

Figure 87. PSRR measurement schematic



5.13 Principle of operation

We fixed the DC voltage supply (V_{cc}), the AC sinusoidal ripple voltage (V_{ripple}) and no supply capacitor C_s is used.

The PSRR value for each frequency is:

$$PSRR(dB) = 20 \times \log_{10} \left[\frac{Rms(V_{ripple})}{Rms(V_{s+} - V_{s-})} \right]$$

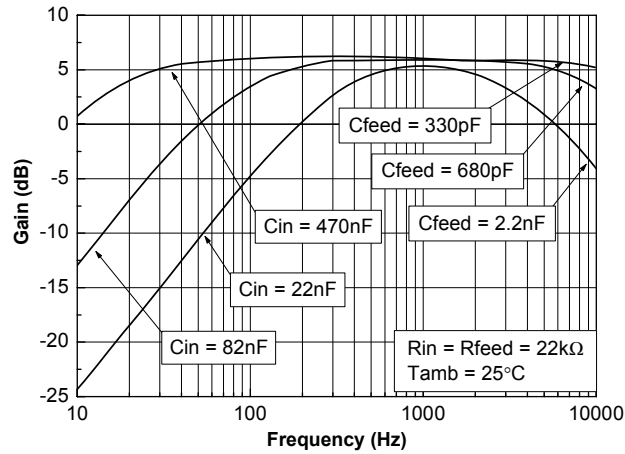
Remark : The measure of the Rms voltage is not a Rms selective measure but a full range (2 Hz to 125 kHz) Rms measure.

It means that we measure the effective Rms signal + the noise.

5.14 High/low cut-off frequencies

For their calculation, please check the figure below:

Figure 88. Frequency response gain vs C_{in} and C_{feed}



6 Package information

In order to meet environmental requirements, ST offers these devices in different grades of **ECOPACK** packages, depending on their level of environmental compliance. ECOPACK specifications, grade definitions and product status are available at: www.st.com. ECOPACK is an ST trademark.

6.1 MiniSO8 package information

Figure 89. MiniSO8 package outline

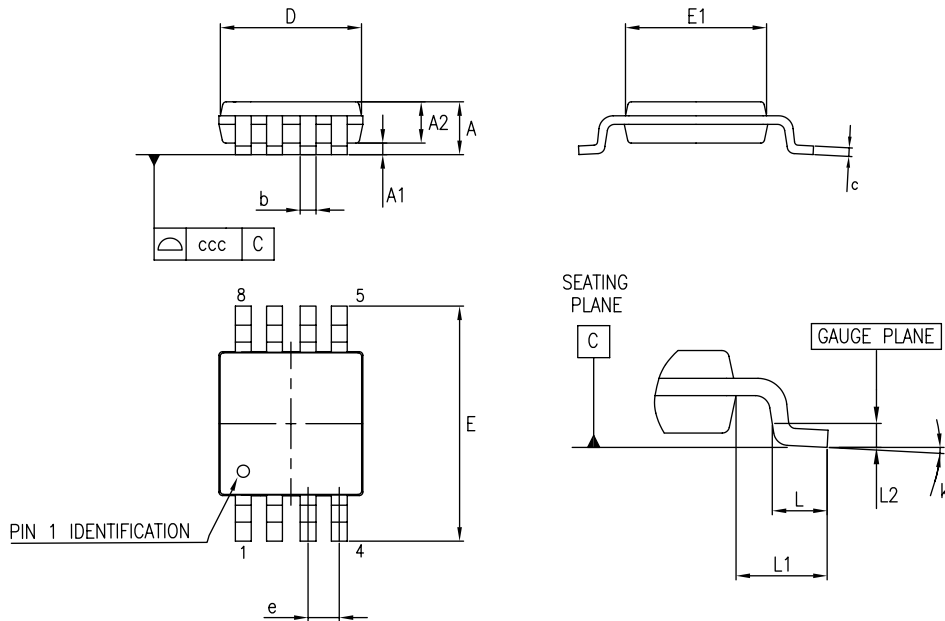


Table 11. MiniSO8 mechanical data

| Dim. | Millimeters | | | Inches | | |
|------|-------------|------|------|--------|-------|-------|
| | Min. | Typ. | Max. | Min. | Typ. | Max. |
| A | | | 1.1 | | | 0.043 |
| A1 | 0 | | 0.15 | 0 | | 0.006 |
| A2 | 0.75 | 0.85 | 0.95 | 0.03 | 0.033 | 0.037 |
| b | 0.22 | | 0.4 | 0.009 | | 0.016 |
| c | 0.08 | | 0.23 | 0.003 | | 0.009 |
| D | 2.8 | 3 | 3.2 | 0.11 | 0.118 | 0.126 |
| E | 4.65 | 4.9 | 5.15 | 0.183 | 0.193 | 0.203 |
| E1 | 2.8 | 3 | 3.1 | 0.11 | 0.118 | 0.122 |
| e | | 0.65 | | | 0.026 | |
| L | 0.4 | 0.6 | 0.8 | 0.016 | 0.024 | 0.031 |
| L1 | | 0.95 | | | 0.037 | |
| L2 | | 0.25 | | | 0.01 | |
| k | 0° | | 8° | 0° | | 8° |
| ccc | | | 0.1 | | | 0.004 |

6.2 SO8 package information

Figure 90. SO-8 package outline

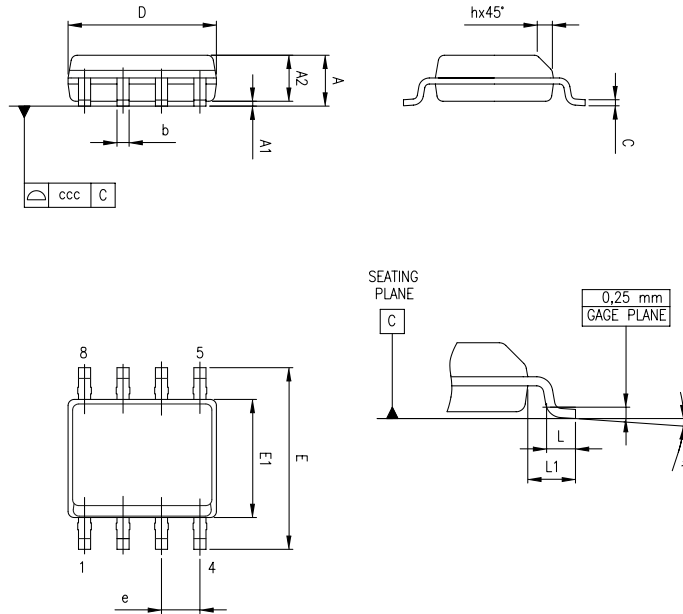


Table 12. SO-8 package mechanical data

| Ref. | Dimensions | | | | | |
|------|-------------|-------|------|--------|-------|-------|
| | Millimeters | | | Inches | | |
| | Min. | Typ. | Max. | Min. | Typ. | Max. |
| A | | | 1.75 | | | 0.069 |
| A1 | 0.10 | | 0.25 | 0.04 | | 0.010 |
| A2 | 1.25 | | | 0.049 | | |
| b | 0.28 | 0.40 | 0.48 | 0.011 | 0.016 | 0.019 |
| c | 0.17 | | 0.23 | 0.007 | | 0.010 |
| D | 4.80 | 4.90 | 5.00 | 0.189 | 0.193 | 0.197 |
| E | 5.80 | 6.00 | 6.20 | 0.228 | 0.236 | 0.244 |
| E1 | 3.80 | 3.90 | 4.00 | 0.150 | 0.154 | 0.157 |
| e | | 1.27 | | | 0.050 | |
| h | 0.25 | | 0.50 | 0.010 | | 0.020 |
| L | 0.40 | 0.635 | 1.27 | 0.016 | | 0.050 |
| L1 | | 1.04 | | | 0.040 | |
| k | 1° | | 8° | 1° | | 8° |
| ccc | | | 0.10 | | | 0.004 |

7 Ordering information

Table 13. Ordering information

| Order code | Temperature range | Package | Packing | Marking |
|------------|-------------------|---------|---------------|---------|
| TS4871IST | -40, +85°C | MiniSO8 | Tape and reel | 4871I |
| TS4871IDT | | SO8 | | 4871 |
| TS4871ID | | SO8 | Tube | 4871 |

Revision history

Table 14. Document revision history

| Date | Revision | Changes |
|-------------|----------|---|
| 08-May-2019 | 9 | No history because of migration. Removed the part number TS4871IQT and all its reference throughout the document. |

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